Appendix F

Sewerage Impact Assessment

Prepared for

Wing Mau Tea House Limited

Prepared by

Ramboll Hong Kong Limited

PROPOSED REZONING FROM "RESIDENTIAL (GROUP B)1" ZONE TO "RESIDENTIAL (GROUP B)4" ZONE FOR MEDIUM-DENSITY HOUSING DEVELOPMENT TO INCLUDE A FOOTPATH FOR PUBLIC USE AT VARIOUS LOTS AND ADJACENT GOVERNMENT LAND IN DD130, LAM TEI, TUEN MUN SEWERAGE IMPACT ASSESSMENT

RAMBOLL

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1. INTRODUCTION

1.1 Background and Objectives

- 1.1.1 The Application Site is located at various lots and adjoining government land in D.D.130, Lam Tei, Tuen Mun.
- 1.1.2 In order to confirm the environmental feasibility of the Proposed Development, Ramboll Hong Kong Limited is commissioned to conduct the Sewerage Impact Assessment based on the information of the Proposed Development.

1.2 Application Site and its Environ

- 1.2.1 With a development area of 8,896m² and zoned as Residential (Group B) 1" (R(B)1) zone, the Application Site is currently a vacant site situated at D.D. 130, Lam Tei bounded by the Castel Peak Road Lam Tei to the east separated by the Tuen Ma Line viaduct and LRT tracks. Existing residential development, Lingrade Garden, is located to the north of the Application Site. Some temporary carpark, open storage and village houses are located to the west of the site separated by a nullah.
- 1.2.2 **Figure 1.1** shows the location of the Application Site and its environ.

1.3 Proposed Development

- 1.3.1 The Proposed Development consists of 5 residential towers ranging from 14 storeys to 27 storeys. A clubhouse is situated below Tower 1 and Tower 3. The number of storeys and building height information of the residential towers are as follow:
 - Tower 1: 27 storeys (+107.8 mPD)
 - Tower 2: 27 storeys (+107.8 mPD)
 - Tower 3: 16 storeys (+66.8 mPD)
 - Tower 4: 14 storeys (+59.8 mPD)
 - Tower 5: 24 storeys (+94.8 mPD)
- 1.3.2 The total numbers of units are 1,385 units with a proposed domestic GFA of 44,480m² (PR5.0). Detailed plans of the Proposed Development are presented in **Appendix 1.1**.



2. SEWERAGE IMPACT ASSESSMENT

2.1 Scope of Work

- 2.1.1 The Application site is currently vacant and there is no public sewer network serving the Application Site and the surrounding environment due to the isolation by a nullah.
- 2.1.2 The aim of this study is to evaluate the sewage flow generated from the Proposed Development and assess whether there is adverse sewerage impacts to the surrounding environment.

2.2 Assessment Criteria and Methodology

- 2.2.1 The Commercial and Industrial Floor Space Utilization Survey (CIFSUS) conducted by the Planning Department has been used to determine the worker density for various economic activities and planned usage types.
- 2.2.2 Environmental Protection Department's (EPD's) Guidelines for Estimating Sewage Flows for Sewage Infrastructure Planning, Version 1 (GESF) is referred to estimate the quantity of the sewage generated from the Proposed Development and the existing development. Sewage flow parameters and global peaking factors in this document are adopted.
- 2.2.3 According to the Table T-1 of the said EPD Guideline, the unit flow factor (UFF) of resident (Private R2) is 0.27 m³/day, while the UFF for employees for the clubhouse is 0.28m³/day.

2.3 Existing Condition

2.3.1 Currently, there are no public sewerage facilities in the vicinity of the Application Site and the extension of the public sewerage system to Application Site is unlikely as the Application Site is separated from the nearest sewerage manhole by a nullah. It will therefore be necessary to provide on-site treatment facilities before discharging the treated effluent into the nearby nullah.

2.4 Future Estimated Flow

2.4.1 Under the current scheme, the Proposed Development will consist of 1,385 residential units, a clubhouse with a size of 2,002 m² and two swimming pools with an area of 48m² and 108m² respectively. Based on such design parameters, the Average Dry Weather Flow (ADWF) excluding the backwash of the swimming pools is estimated to be 1,028.2 m³/day, as tabulated in **Table 2.1** below and **Appendix 2.1**.

| Table 2.1 | Estimated Sewage Flow from the Proposed Development |
|-----------|---|
|-----------|---|

| | | | Remarks |
|-----------------------------------|---|---------|---|
| Residential Use | | | |
| Total number of residential units | = | 1,385 | |
| Total number of residents | = | 3,740 | people (average household size of 2.7 is assumed) |
| Design flow | = | 270 | litre/person/day (Private R2 in Table T-1 of GESF) |
| Sewage Generation Rate | = | 1,009.7 | m³/day |
| Clubhouse | | | |



| | | | Remarks |
|---|--------|-------|--|
| Total GFA | = | 2,002 | m ² |
| Assumed floor area per employee | = | 30.3 | m ² per employee (refer to Table 8 of CIFSUS - Community, Social & Personal Services) |
| Total number of employees | | 66 | employees |
| Design flow | = | 280 | litre/employee/day (refer to Table T-2 of GESF - J11 Community, Social & Personal Services) |
| Sewage Generation Rate | = | 18.5 | m³/day |
| Proposed Adult Swimmin | g Poo | | |
| Assumed area of swimming pool | = | 108 | m² |
| Average depth of water | | 1.2 | m |
| Volume of swimming pool | = | 129.6 | m ³ |
| Turnover rate | = | 6 | hr |
| Surface loading rate of filter | = | 50 | m³/m²/hr |
| Filter areas required | | 0.4 | m ² (Volume of Swimming Pool/Turnover Rate/ Surface Loading Rate of Filter) |
| Backwash duration | = | 30 | min/d |
| Backwash flow rate | = | 30 | m³/m²/hr |
| Design flow for swimming pool backwashing | = | 6.5 | m³/day (Backwash flow rate x Filter areas required x Backwash duration) |
| Design flow for swimming pool backwashing | = | 0.08 | litre/sec |
| Proposed Children Swimn | ning P | ool | |
| Assumed area of swimming pool | = | 48 | m ² |
| Average depth of water | | 1.2 | m |
| Volume of swimming pool | = | 57.6 | m ³ |
| Turnover rate | = | 6 | hr |
| Surface loading rate of filter | = | 50 | m³/m²/hr |
| Filter areas required | | 0.2 | m ² |



| | | | Remarks |
|---|-------|------------|--|
| | | | (Volume of Swimming Pool/Turnover Rate/ Surface Loading Rate of Filter) |
| Backwash duration | = | 30 | min/d |
| Backwash flow rate | = | 30 | m³/m²/hr |
| Design flow for swimming pool backwashing | = | 2.9 | m ³ /day (Backwash flow rate x Filter areas required x Backwash duration) |
| Design flow for swimming pool backwashing | = | 0.03 | litre/sec |
| Total Flow from the Propo | sed D | Developmen | t |
| Flow Rate | = | 1,028.2 | m³/day |
| Flow Rate with P _{CIF} (Tuen Mun – 1.1) | = | 1131.0 | m ³ /day (refer to Table T-4 of GESF - Tuen Mun - 1.1) |
| Contributing Population | = | 4189 | people |
| Peaking factor | = | 4.0 | (refer to Table T-5 of GESF for a population of <10,000 incl. stormwater allowance) |
| Peak flow (excluding backwash of all pools) | = | 52.4 | litre/sec |
| Peak flow (including backwash of all pools) | = | 52.5 | litre/sec |

2.5 Proposed Sewage Treatment Facility

- 2.5.1 As the Application Site is not served by public sewerage system currently, it is proposed to provide on-site sewage treatment to ensure sewage can be discharged in a proper manner. Once public sewerage system is connected to the Application Site, the sewage flow from the proposed development may be discharged to the public sewerage system in the future.
- 2.5.2 The use of Sewage Treatment Plant (STP) is recommended for the Proposed Development. The "Guidelines for the Design of Small Sewage Treatment Plants" published by the EPD for the design, construction, operation and maintenance of STP should be followed. The effluent should be treated to acceptable standards as stated in "Technical Memorandum Standards for Effluents Discharged into Drainage and Sewerage systems, Inland and Coastal waters". As the proposed development have a population of more than 2,000, the Applicant will approach EPD to discuss the design of the STP during detailed design stage.
- 2.5.3 Suitable treatment for the sewage generated by the proposed development could practically be provided by a package treatment unit, i.e. treatment facilities which are supplied and installed as complete units, including all treatment stages. For example, one appropriate technology would be Membrane Bioreactor (MBR) units, followed by disinfection to achieve the required effluent standards. The treated effluent can then be discharged of into the drainage system. A sample of the MBR unit is enclosed in **Appendix 2.2**.



- 2.5.4 The design and operation of the STP will be in accordance with the "Guidelines for Design of Small Sewage Treatment Plants" published by the EPD, with adequate capacity to handle three times of ADWF. The area of the STP will be approximately 1,254m² occupying two basement floors. The treated effluent would then be discharged into a new drainage pipe connecting to the existing nullah to the west of the Application Site. **Figure 2.1** shows the indicative location of the on-site treatment plant and the capacity checking of the pipe discharging into the nullah is also presented in **Appendix 2.1**. The exact discharge location and pipe design will be subject to further study and agreed with EPD during detailed design stage.
- 2.5.5 The effluent generated from the Proposed Development will go through the process of disinfection to achieve the necessary discharge standards as set out in EPD's Technical Memorandum Standards for Effluents Discharged into Drainage and Sewerage Systems, Inland and Coastal Waters (Table 10b Standards for Effluents Discharged into the marine waters of Southern, Mirs Bay, Junk Bay, North Western, Eastern Buffer and Western Buffer Water Control Zone).
- 2.5.6 As a good practice for sewage treatment facilities, measures will be incorporated into the design to minimise the risk of emergency overflow from the treatment plant. These measures include standby pumps, secure power supplies, appropriate alarms, as well as comprehensive Operation and Maintenance procedures in order to keep the facilities in good working order.
- 2.5.7 The proposed on-site MBR will be fully enclosed with deodorising system, so that the noise and odour emitted from the plant will not have adverse impact upon the surrounding residents.
- 2.5.8 The project proponent will be responsible for the implementation and maintenance of the proposed STP and arrangement of the sludge from the proposed STP.
- 2.5.9 The detailed design and size of the MBR unit will be provided in later stage for EPD's approval.



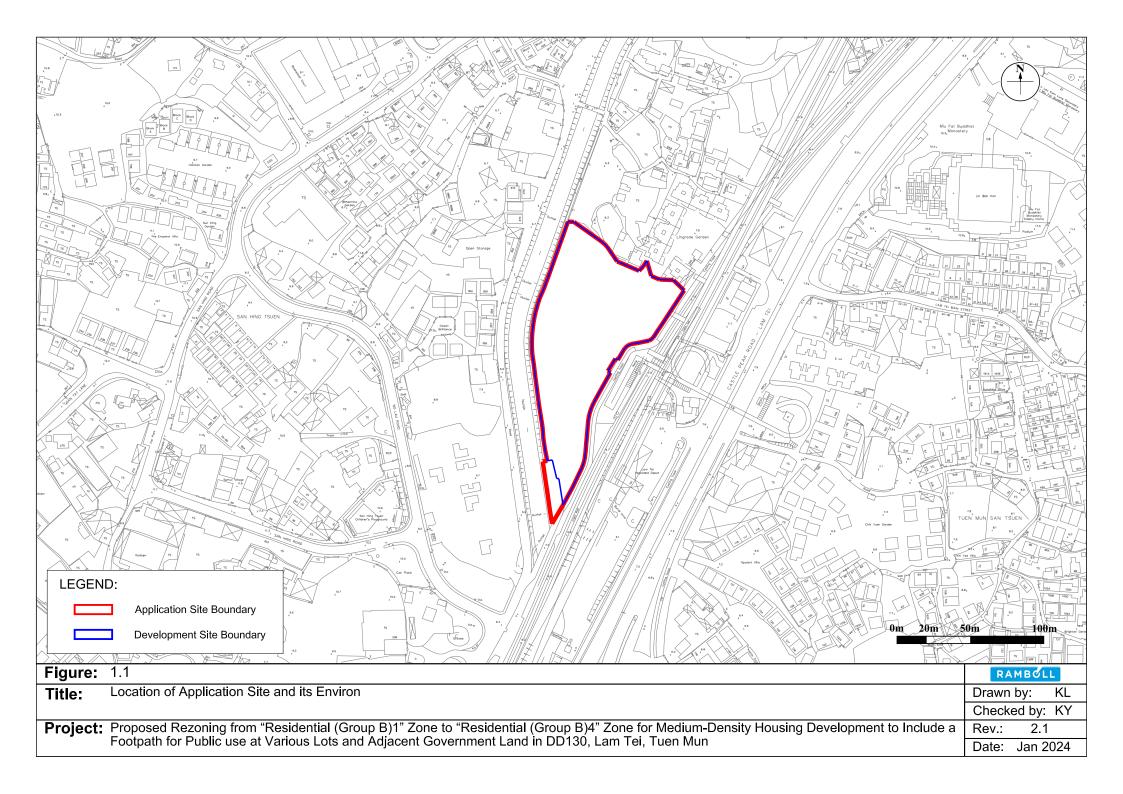
3. CONCLUSION

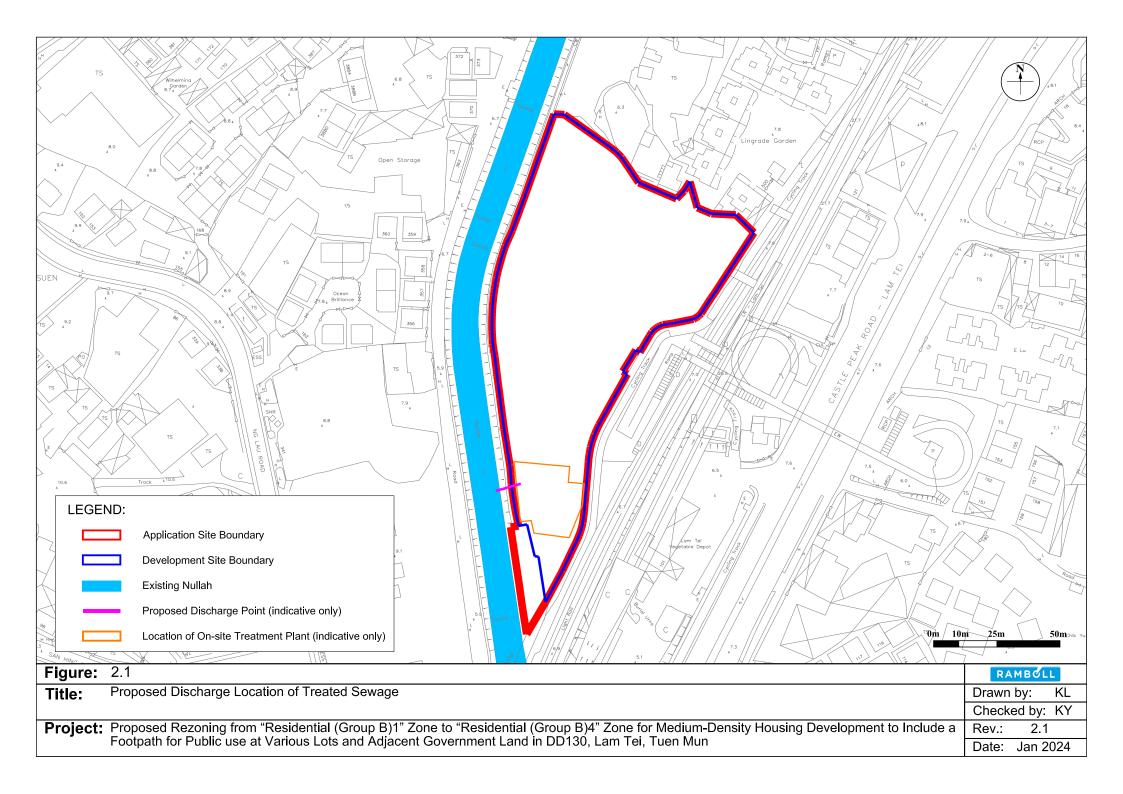
- 3.1.1 A residential development is proposed for the Application Site at D.D.130 Lam Tei, Tuen Mun. The potential sewerage impact has been quantitatively addressed.
- 3.1.2 Since there is no public sewerage system available for the Proposed Development, onsite treatment will be required. Connection to the public sewer will be a long-term option after availability of trunk sewer connecting to the Application Site.
- 3.1.3 An on-site treatment with Membrane Bioreactor (MBR) will be used to treat effluent from the Proposed Development, discharge the treated effluent to the nearby nullah. Relevant statutory guidelines and regulations will be followed and detail design of the MBR unit will be provided in later stage.
- 3.1.4 With the sewage treatment plant and proper maintenance in place, it is concluded that the Proposed Development will not have any unacceptable adverse sewerage impact to the surrounding.



Figures



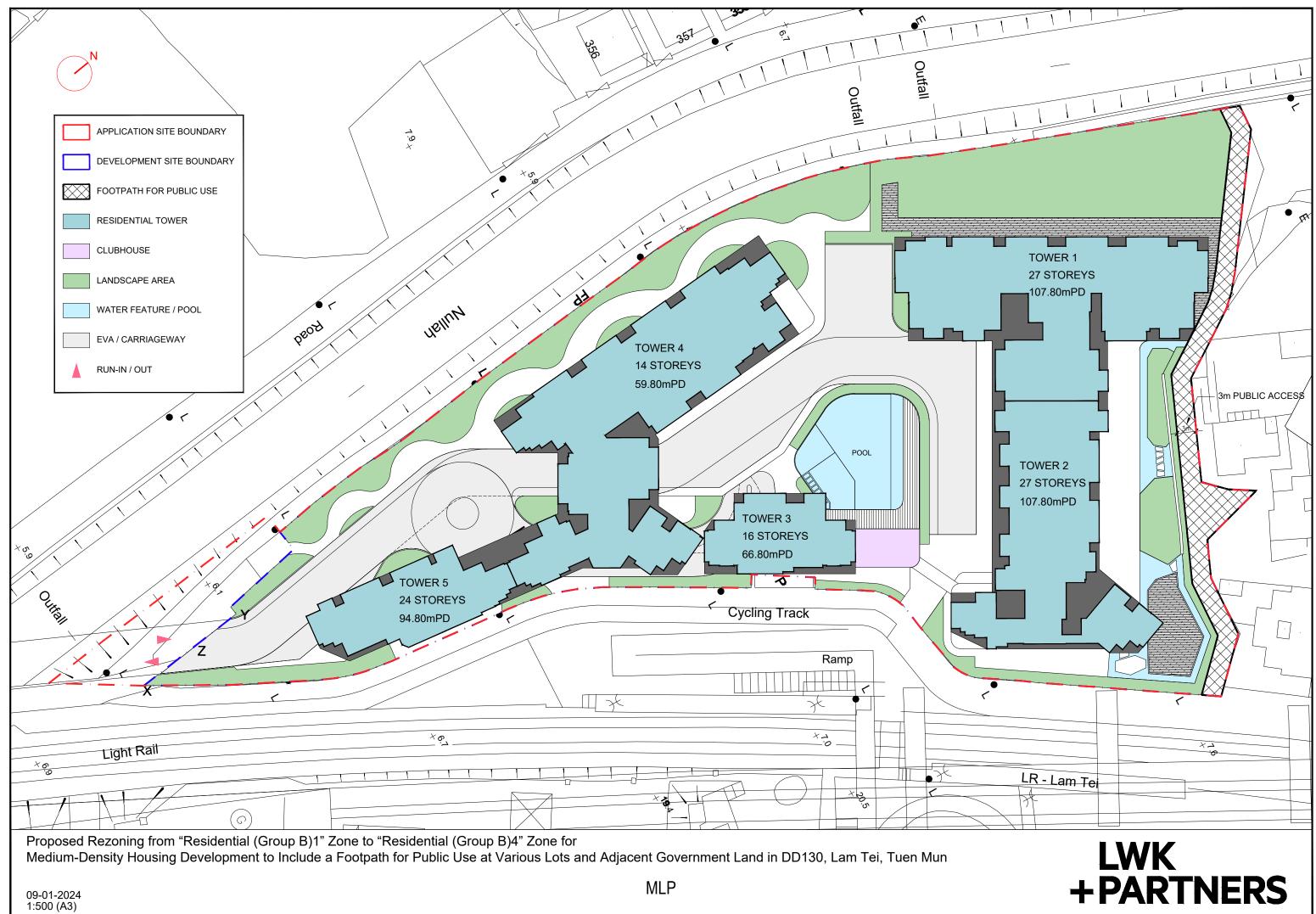


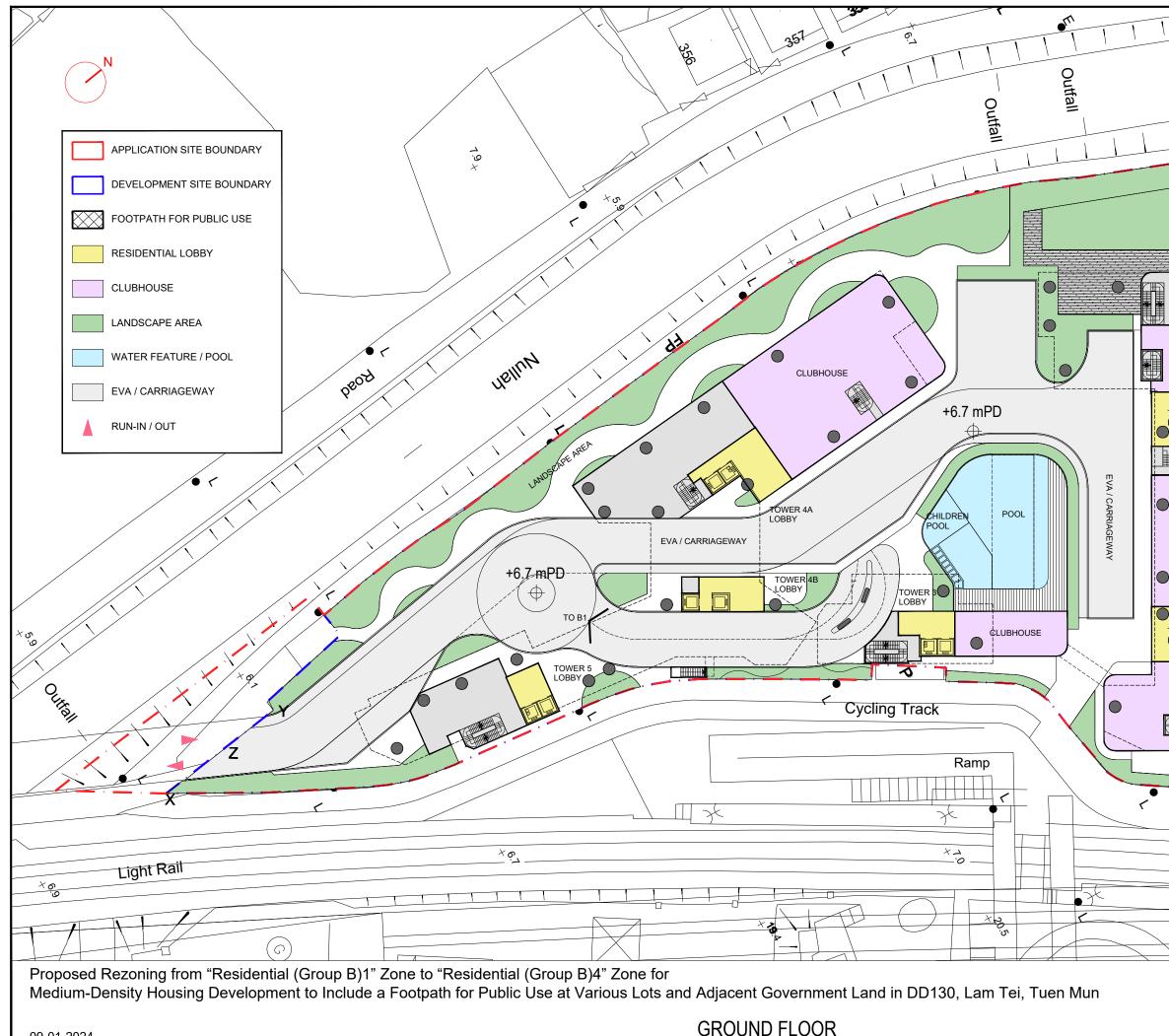


Appendix 1.1

Detailed Layout Plans of the Proposed Development

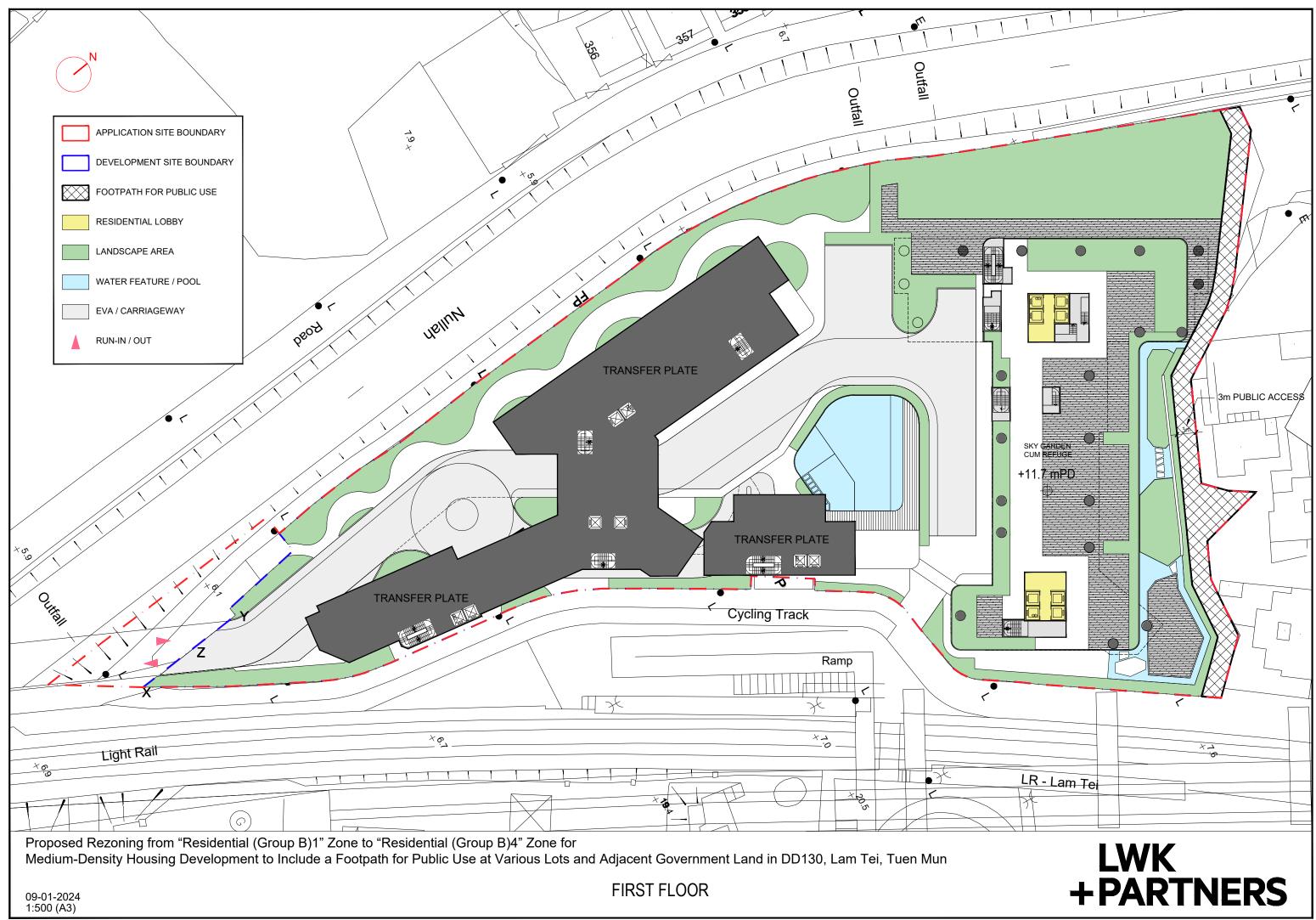




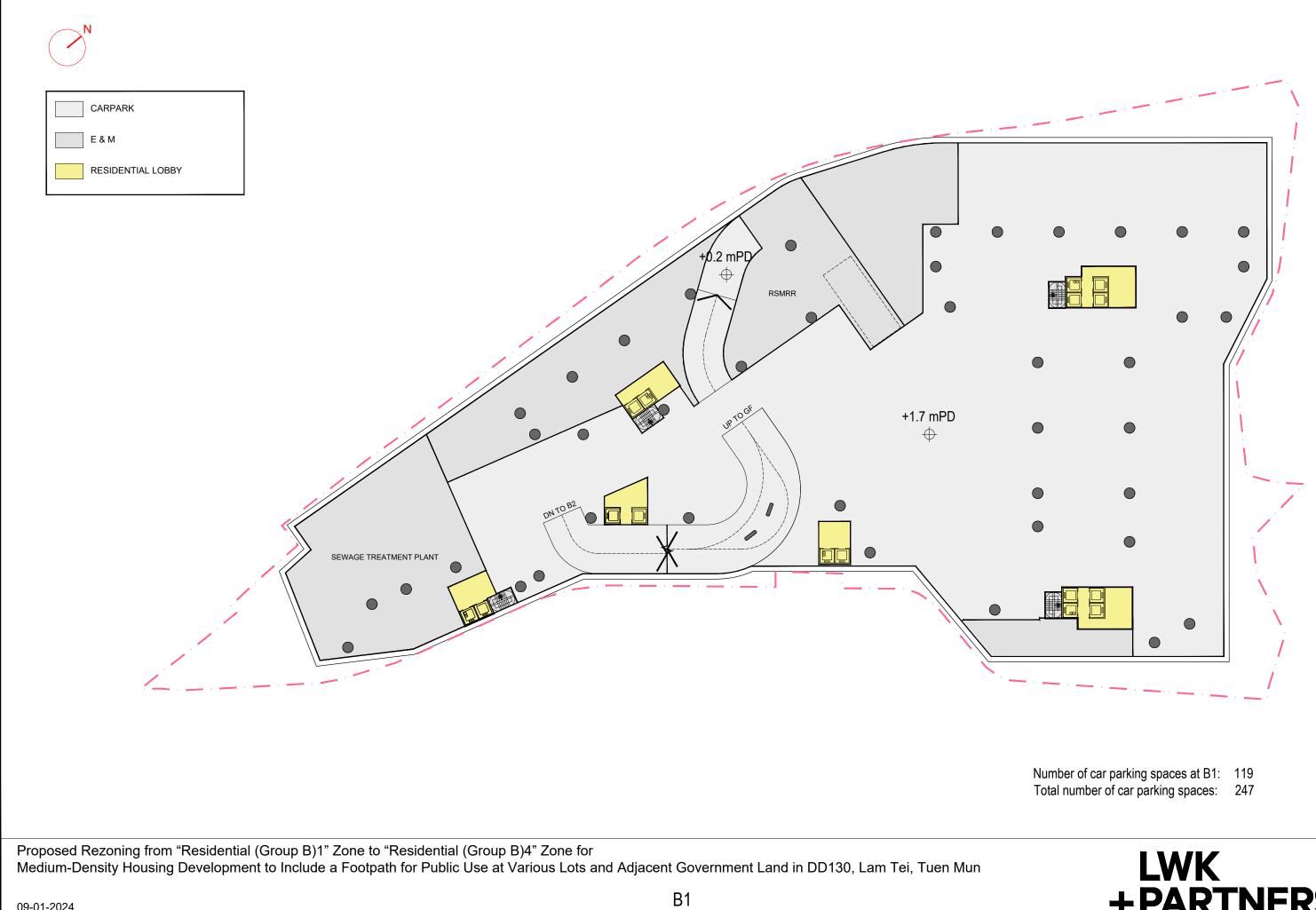


GROUND FLOOR

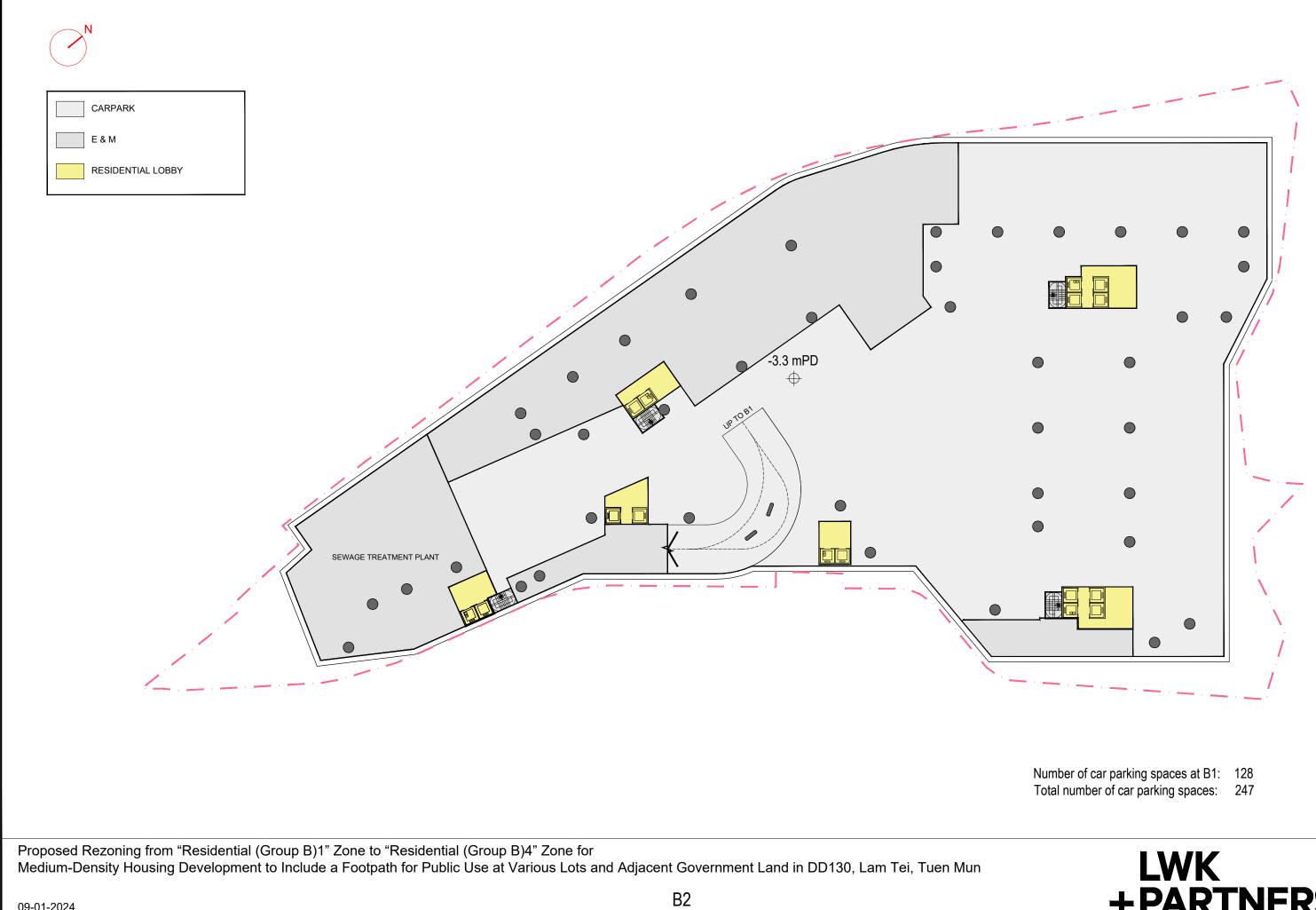
LANDSCAPE AREA • TOWER 1 LOBBY 3m PUBLIC ACCES CLUBHOUSE TOWER 2 LOBBY < XJ LR - Lam Tei LWK **+PARTNERS**



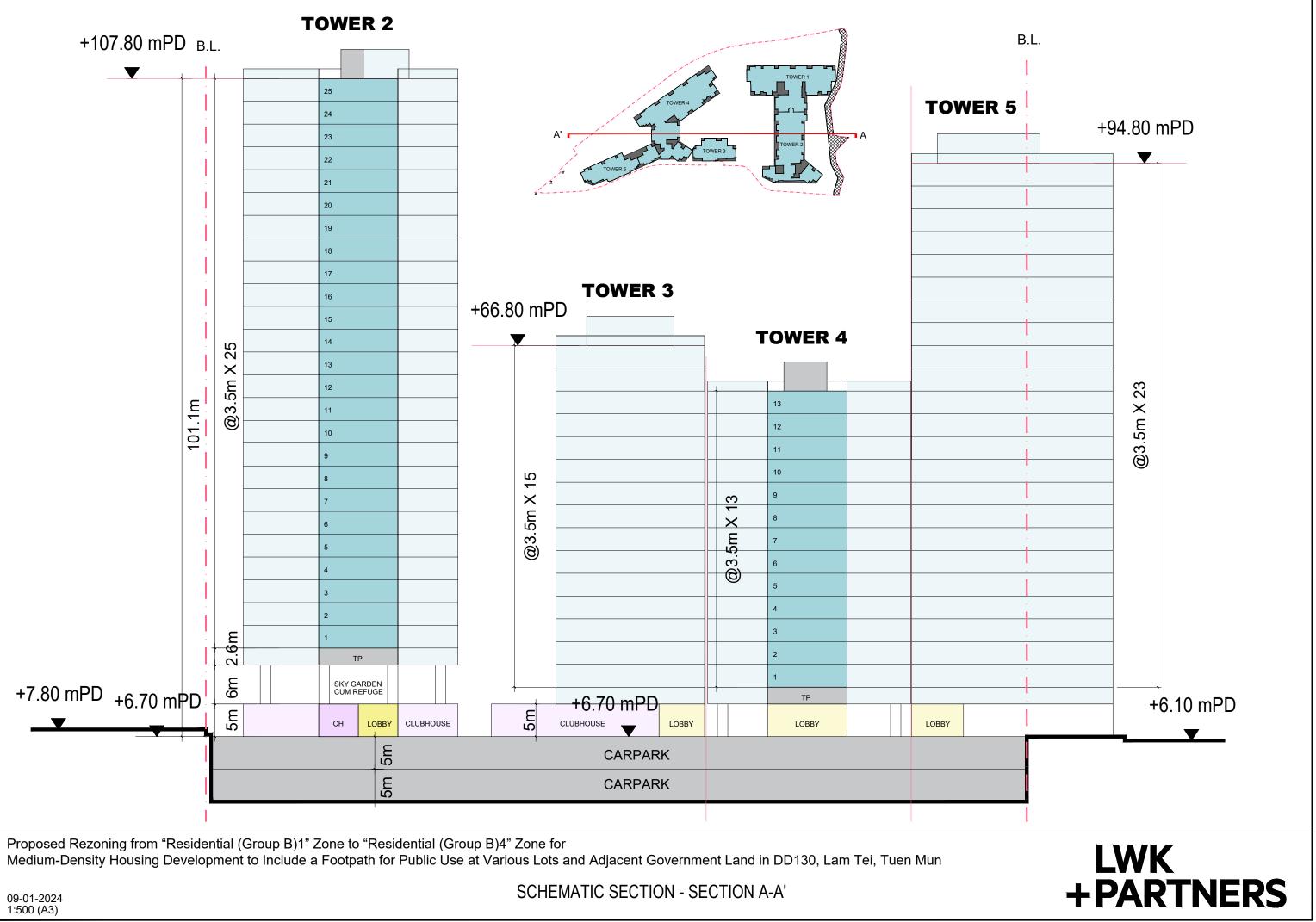
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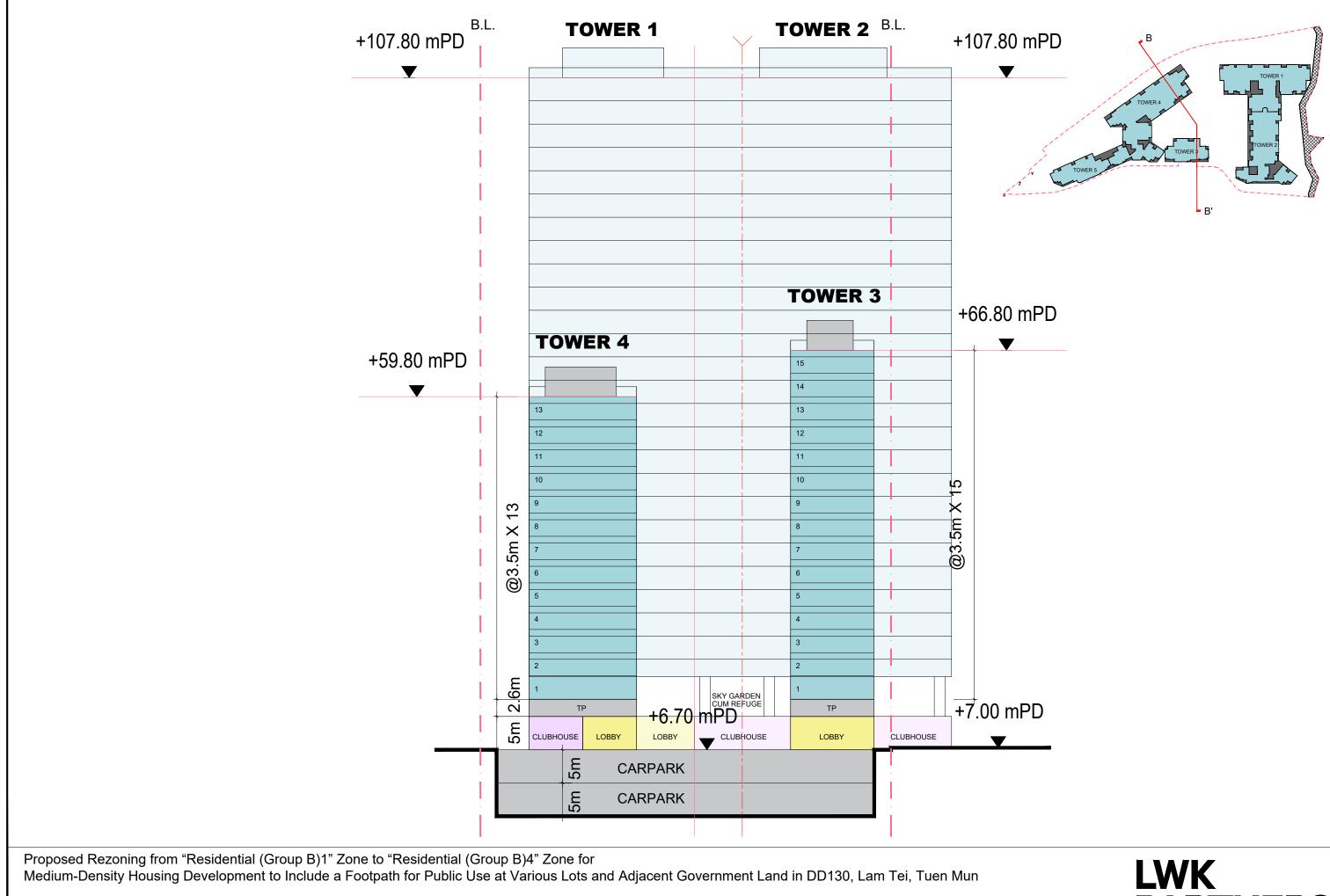


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+PARTNERS





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SCHEMATIC SECTION - SECTION B-B'

+PARTNERS

Appendix 2.1

Detailed Sewerage Impact Assessment Calculations



Table 1 Calculation for Sewage Generation Rate of the Proposed Development at the Application Site

| Residential Units | | |
|---|---|---|
| Total number of residential units | = | 1,385 units |
| Total number of residents | = | 3739.5 residents (2.7 people per flat is assumed) |
| Design flow | = | 270 litre/person/day (Private R2 in Table T-1 of GESF) |
| Sewage generation rate | = | 1,009.7 m³/day |
| | | |
| Clubhouse | | |
| Total GFA | = | 2,002 m ² |
| Assumed floor area per employee | = | 30.3 m ² per employee (refer to Table 8 of CIFSUS - Community, Social & Personal Services) |
| Total number of employees | = | 66 employees |
| Design flow for employees | = | 280 litre/employee/day (refer to Table T-2 of GESF - J11 Community, Social & Personal Services) |
| Sewage generation rate | = | 18.5 m³/day |
| Proposed Adult Swimming Pool | | |
| | = | 108 m ² |
| Assumed area of swimming pool Average depth of water | = | 1.2 m |
| o . | = | 129.6 m ³ |
| Volume of swimming pool Turnover rate | = | 6 hr |
| | | $50 \text{ m}^3/\text{m}^2/\text{hr}$ |
| Surface loading rate of filter | = | 0.4 m^2 |
| Filter areas required | = | |
| Backwash duration | = | 30 min/d |
| Backwash flow rate | = | $30 \text{ m}^3/\text{m}^2/\text{hr}$ |
| Design flow for swimming pool backwashing | = | 6.5 m ³ /day |
| Design flow for swimming pool backwashing | = | 0.08 litre/sec |
| Proposed Children Swimming Pool | | |
| Assumed area of swimming pool | = | 48 m ² |
| Average depth of water | = | 1.2 m |
| Volume of swimming pool | = | 57.6 m ³ |
| Turnover rate | = | 6 hr |
| Surface loading rate of filter | = | $50 \text{ m}^3/\text{m}^2/\text{hr}$ |
| Filter areas required | = | 0.2 m ² |
| Backwash duration | = | 30 min/d |
| Backwash flow rate | = | $30 \text{ m}^3/\text{m}^2/\text{hr}$ |
| Design flow for swimming pool backwashing | = | 2.9 m ³ /day |
| Design flow for swimming pool backwashing | = | 0.03 litre/sec |
| besign new for swimming peer backwashing | | |
| Total Flow from the Proposed Development | | |
| Flow rate (excluding backwash of all pools) | = | 1,028.2 m³/day |
| Flow rate with P _{CIF} (Tuen Mun - 1.1) | = | 1131.0 m ³ /day (refer to Table T-4 of GESF - Tuen Mun - 1.1) |
| Contributing population | = | 4189 people |
| Peaking factor | = | 4.0 (refer to Table T-5 of GESF for a population of <10,000 incl. stormwater allowance) |
| Peak flow (excluding backwash of all pools) | = | 5.2.4 litre/sec |
| Peak flow (including backwash of all pools) | | 52.5 litre/sec |
| reak new (including backwash or all pools) | | <u></u> |

Remarks:

(1) For job type J11, the "per-employee" unit flow factor takes into account the flows of customers and tenants.

Table 2 Hydraulic Capacity of Proposed Drainage Pipe for Onsite Sewage Treatment Plant

| Segment | Manhole | Manhole | Motorial | Pipe Dia. | Pipe Length | g | k _s | S | V | V | Area | Q | Estimated Capacity |
|---------|-----------|-----------|----------|-----------|-------------|---------|----------------|-------|----------|------|----------------|-------------------|--------------------|
| Segment | Reference | Reference | Material | mm | m | m/s^2 | m | | m²/s | m/s | m ² | m ³ /s | L/s |
| - | STP | Nullah | Clayware | 350 | 10.30 | 9.81 | 0.0030 | 0.003 | 0.000001 | 0.74 | 0.10 | 0.07 | 71 |

(1) g=gravitational acceleration; k_s =equivalent sand roughness; s=gradient; v=kinematic viscosity of water; V=mean velocity Remarks:

(2) According to Section 5.1.2 of SDM, gradient of at least 1: DN (i.e. Nominal diameter of the sewer in mm) is adopted.

(3) The values of ks = 3.0mm is used for the calculation of slimed <u>clayware</u> sewer, poor condition @mean velocity = approximately 0.75m/s (based on Table 5: Recommended Roughness Values in Sewerage Manual)

(4) The value of velocity (V) is referred to the Tables for the hydraulic design of pipes, sewers and channels (8th edition)

(5) Equation used: $V = -\sqrt{(8gDs)}\log(\frac{k_s}{3.7D} + \frac{2.51v}{D\sqrt{(2gDs)}})$

| Table 3 Capacity Checking for the | | |
|---|-------------------------------|-----------------------------------|
| 130003130321101000000000000000000000000 | Uranacaa urainada Uina at tha | I INCITA SAMIARA I RAATMANT DIANT |
| | | |
| | | |

| Segment | Reference | Manhole Reference | Pipe Dia. (mm) | Pipe Length (m) | Gradient | Estimated Capacity (L/s) | from the Proposed | (%) | Status |
|---------|-----------|----------------------|----------------------|-----------------------|----------|-----------------------------|----------------------|-------|--------|
| - | STP | Nullah | 350 | 10.3 | 0.003 | 71 | 52.4 | 74.0% | OK |

Appendix 2.2

Sample of Membrane Bioreactor



In conventional activated sludge processes, separation of treated water from the sludge is mainly achieved by sedimentation in secondary clarification tank. This requires a considerable amount of space and capital cost, and separation efficiency is low.

Using membrane to replace the secondary clarification tank, suspended solids can be completely removed from treated water, resulting in a high effluent quality. It not only concentrates slow-growing bacteria, but also retains large molecular organic compounds in reactor, thereby increasing contact time with the sludge. Thus, removal rate of COD, BOD, nitrogen and phosphorus will be greatly increased.



Raw wastewater (left) and treated water (right)

MBR Membrane Bio-Reactor

- Wastewater Reuse
- High Strength Wastewater Treatment
- Excellent Effluent Quality

Advantanges of MBR

- 1 High effluent quality
 - · Permeate free of suspended solids
- 2 Small footprint, elimination of secondary clarification tank · Only half of the area of conventional activated sludge process is required, and capital cost is reduced · Solve the problem of poor sedimentation in conventional activated sludge process; especially for winter
- 3 Long solid retention time, easy management · Sludge wasting volume is greatly reduced
- 4 High biomass concentration and treatment efficiency · Operate at biomass concentration of 10,000 - 20,000 mg/L, COD removal and denitrification occur simultaneously
- 5 Easy to install in the existing aeration tank to become a MBR system
- 6 Easy for operation & maintenance
- 7 Greatly reduce the volume of aeration tank
- Reduce fouling and increase water flux 8

Case Studies

| Wastewater Source | Parameters | Influent | Effluent | Removal Rate (%) |
|---|--------------|----------|----------|------------------|
| Food Processing | BOD (mg/L) | 1590 | 1 | 99.9 |
| , et al. et et et al. et al | CODcr (mg/L) | 2600 | 7 | 99.0 |
| 3 | SS/ (mg/L) | 380 | <1 | 100 |
| Sauce Production | BOD (mg/L) | 3630 | 5 | 99.9 |
| | SS/ (mg/L) | 380 | <1 | 100 |
| Landfill Leachate | CODcr (mg/L) | ~10,000 | 60 | 99.4 |
| | SS/ (mg/L) | <500 | <1 | 100 |
| Grey Water Recycling | BOD (mg/L) | <=200 | <=10 | 95.0 |
| | SS/ (mg/L) | <=200 | < 1 | 100 |

Uses of MBR

- 1 Domestic wastewater treatment / Grey water recycling High treatment efficiency, high effluent quality
- 2 Industrial wastewater treatment Suitable for landfill leachate, high BOD food processing wastewater, livestock wastewater, chemical wastewater and pulp and paper wastewater
- Water reuse or recycling 3 Direct reuse or purified with reverse osmosis

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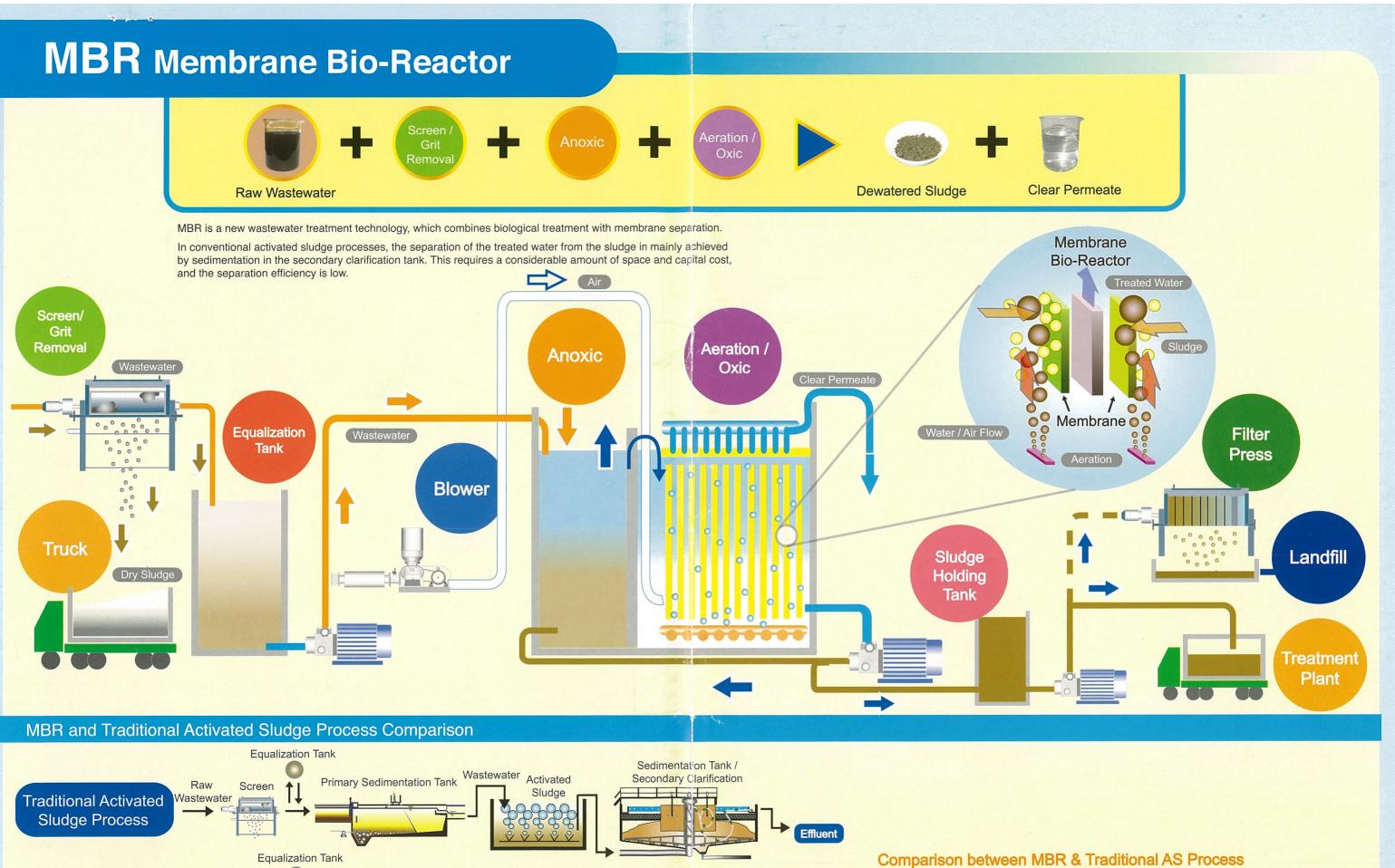
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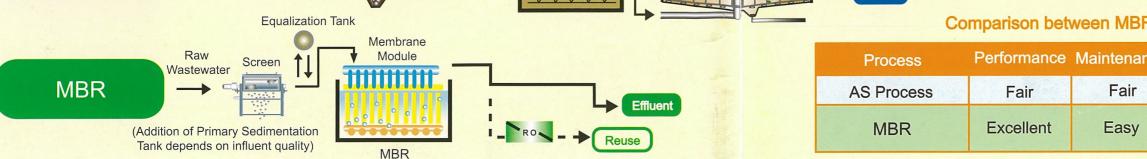
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| nce | Sludge Conc. | Space Saving | Direct Reuse |
|-----|--------------|--------------|--------------|
| | Low | Fair | No |
| | High | Yes | Yes |