Attachment 7 –

**Drainage Impact Assessment** 

PROPOSED COMPOSITE "SOCIAL WELFARE FACILITY (RESIDENTIAL CARE HOME FOR THE ELDERLY)" (RCHE) AND "RESIDENTIAL INSTITUTION" (SENIOR HOSTEL) DEVELOPMENT ON A SITE CURRENTLY ZONED AS "GOVERNMENT, INSTITUTIONAL OR COMMUNITY" (G/IC) IN LOT NOS. 257 (PART), 258 RP (PART) AND ADJOINING GOVERNMENT LAND IN D.D. 122, PING SHAN, YUEN LONG

## DRAINAGE IMPACT ASSESSMENT

Feb 2024

Report No: RT23042-DIA-01\_v1

## Submitted to:

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Project:	HOME FOR THI HOSTEL) DEVE INSTITUTIONA (PART) AND AE LONG	OMPOSITE "SOCIAL WELFARI E ELDERLY)" (RCHE) AND "RES ELOPMENT ON A SITE CURRE L OR COMMUNITY" (G/IC) IN DJOINING GOVERNMENT LANI CTASSESSMENT	IDENTIAL NTLY ZON LOT NO	INSTITUTIC IED AS "GO' S. 257 (PAF	N" (SENIOR VERNMENT, RT), 258 RP
Report No.:	RT23042-DIA-01_	_v1			
Revision	Issue Date	Description	Author	Checker	Approver
0	11/01/2024	Issued for Comment	ксс	ZC	НМ
1	02/02/2024	Issued for Comment	ксс	ZC	НМ
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Director

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## 1 INTRODUCTION

## 1.1 PROJECT BACKGROUND

- 1.1.1. The Joint Great Properties Limited (the Project Proponent) is proposed to develop a composite social welfare facility for Residential Care Home for the Elderly (RCHE) and residential institution for senior hostel at Lot Nos. 257 (Part), 258 RP (Part) and adjoining government land in D.D. 122, Ping Shan, Yuen Long (hereafter refer to the Proposed Development).
- 1.1.2. BeeXergy Consulting Limited (BXG) was commissioned by DeSpace (International) Limited (Project Planner) to conduct a Drainage Impact Assessment (DIA) for the Proposed Development to support the application under Section 16 of the Town Planning Ordinance. Latest architectural drawings of the Proposed Development and technical information of the Project Site were largely provided by the Project Planner and Project Architect.

## 1.2 PROJECT LOCATION

1.2.1. The Application Site is located at Ping Shan North in Yuen Long district, bounded by warehouses to the North, East, and South. **Figure 1.1** shows the location of the Application Site, Project Site, and its environs.

## 1.3 APPLICATION SITE AND PROPOSED DEVELOPMENT

- 1.3.1. The Application Site is approximately 3,300m² while the Project Site is approximately 2,114m² within the Application Site.
- 1.3.2. The Application Site is currently zoned as "Government, Institution or Community" and surrounded by "Green Belt" and "Village Type Development" under the Approved Ping Shan Outline Zoning Plan (OZP) No. S/YL-PS/20.
- 1.3.3. The Proposed Development is an 8-storey building consisting of senior hostel, dormitory, rehabilitation area, activity rooms, offices, kitchen, laundry, and carpark. An access road will be constructed from the Project Site and connected to Tsui Sing Road. The Master Layout Plan provided by the Project Architect is enclosed in **Appendix A**.

## 2 DRAINAGE IMPACT ASSESSMENT

## 2.1 SCOPE OF WORKS

2.1.1. The objectives of this DIA are to assess whether the Proposed Development may cause adverse impacts on drainage and flooding or not and to recommend appropriate mitigation measures to alleviate unacceptable drainage impact, if any.

## 2.2 SITE LOCATION AND TOPOGRAPHY

2.2.1. The Application Site is located at Ping Shan North with a hill at approximately +30.6mPD to the North West according to topography from Lands Department (LandsD). The Application Site is currently occupied by warehouses with public drainage and village drainage system nearby. The location of the existing drainage system is shown in Appendix B.

## 2.3 DRAINAGE ANALYSIS

- 2.3.1. Peak instantaneous runoff before and after the Proposed Development is calculated based on the Rational Method. The recommended physical parameters, including runoff coefficient (C) and storm constants (a, b, c) for different return periods, are referred to the Drainage Services Department (DSD)'s Stormwater Drainage Manual Fifth Edition, January 2018 and Stormwater Drainage Manual Corrigendum No. 1/2022 (SDM).
- 2.3.2. The Rational Method (Equation 1) has been adopted for hydraulic analysis and the peak runoff is given by the following expression:

$$Q_p = 0.278CiA$$
 (Equation 1)

Where:

Q<sub>p</sub> = peak runoff in m<sup>3</sup>/s

C = runoff coefficient

i = rainfall intensity in mm/hr

A = catchment area in km<sup>2</sup>

2.3.3. Rainfall intensity is calculated using the following expression (Equation 2):

$$i = \frac{a}{(t_d + b)^c}$$
 (Equation 2)

Where:

i = rainfall intensity in mm/hr

 $t_d$  = duration in minutes ( $t_d \le 240$ )

a, b, c = storm constants given in Table 3a and Figure 3 of the SDM with return period of 50 years of the HKO Headquarters

2.3.4. For a single catchment, duration (t<sub>d</sub>) can be assumed to be the time of concentration (t<sub>c</sub>) which is calculated as follows (Equation 3):

$$t_c = t_0 + t_f$$
 (Equation 3)

Where:

 $t_c$  = time of concentration (time needed for water to flow overland from the most remote point in a catchment to its outlet)

 $t_0$  = inlet time

 $t_f$  = flow time

2.3.5. Generally,  $t_0$  is much smaller than  $t_f$ . As shown in Equation 2 above,  $t_d$  is the divisor. Therefore, the larger  $t_d$  will result in the smaller rain intensity (i) as well as a smaller  $Q_p$ . For the worst-case scenario (Equation 4 and Equation 5),  $t_0$  is assumed to be negligible and so:

$$t_d = t_c = t_0$$
 (Equation 4)

$$t_c = \frac{0.14465L}{H^{0.2}A^{0.1}}$$
 (Equation 5)

Where:

A = catchment area (m<sup>2</sup>)

H = average slope (m per 100m), measured along the line of natural flow, from the summit of the catchment to the point under consideration

L = distance (on plan) measured on the line of natural flow between the summit and the point under consideration (m)

2.3.6. The capacities of the drainage pipes have been calculated using the Colebrook-White Equation (Equation 6), assuming full bore flow with no surcharge, as follows, incorporate 10% sedimentation in the calculation of drainage flow capacity in accordance with the SDM:

$$V = -\sqrt{32gRs} \times \log\left(\frac{k_s}{14.8R} + \frac{1.25v}{R\sqrt{32gRs}}\right)$$
 (Equation 6)

Where:

V = mean velocity (m/s)

g = gravitation acceleration (m/s<sup>2</sup>)

R = hydraulic radius (m)

k<sub>s</sub> = hydraulic pipeline roughness (m)

V = kinematic viscosity of fluid (m<sup>2</sup>/s)

S = hydraulic gradient (energy loss per unit length due to friction)

## 2.4 CHANGES IN SURFACE CHARACTERISTICS

2.4.1. The Proposed Development is an 8-storey building consisting of senior hostel, dormitory, rehabilitation area, activity rooms, offices, kitchen, laundry, and carpark. An access road will be constructed from the Project Site and connected to Tsui Sing Road. The changes in surface characteristics of the Application Site are shown in Figure 2.1 and summarized in Table 2.1.

**Table 2.1 Changes in Surface Characteristics of the Application Site** 

Scenario of Project	Surface Characteristics (Paved)	Surface Characteristics (Unpaved)
Before Development	89%	11%
After Development	100%	0%

## 2.5 CHANGES IN FLOW CHARACTERISTICS

- 2.5.1. Before Development, the runoff from the Project Site will be discharged to the downstream Stormwater Inlet SIH1007504 via the existing village channel. In contrast, the runoff from the remaining area of the Application Site will be discharged to the downstream Box Culvert SBP1006180 via the existing U-channel SUP1009961.
- 2.5.2. Upon the completion of the Proposed Development, the discharge from the Project Site to the existing village channel will be terminated. The runoff from the Project Site will be collected at the Proposed Terminal Manhole PTM1 and discharged to the Proposed Terminal Manhole PTM4 via the Proposed 375mm circular pipes. The runoff from the access road will be collected by the Proposed 600mm U-channels and discharged to the Proposed Terminal Manhole PTM4. All the runoff from the Application Site will be discharged to the Box Culvert SBP1006180 via the Proposed 400mm circular pipes.
- 2.5.3. Part of the existing U-channel SUP1009961 is located within the Application Site. Those sections (~24m) will be reinstated with covers after the construction of the access road.

2.5.4. The locations of proposed manholes, catchpits, and their connections are shown in **Figure 2.2**.

## 2.6 **CUMULATIVE RUNOFF**

- 2.6.1. Before Development, the Stormwater Inlet SIH1007504 will collect the runoff from the Project Site and its associated upstream catchments, while the Box Culvert SBP1006180 will collect the runoff from the remaining area of the Application Site and its associated upstream catchments.
- 2.6.2. After Development, the Stormwater Inlet SIH1007504 will no longer collect the runoff from the Project Site. All the runoff from the Application Site will be collected by Box Culvert SBP1006180. The changes in cumulative runoff at the Box Culvert SBP1006180 are summarized in **Table 2.2** and the location of catchments after Development is shown in **Figure 2.3**.

Table 2.2 Changes of Cumulative Runoff at Box Culvert SBP1006180

Catchment	Before Dev	elopment*	After Deve	elopment		
	Unpaved Area	Paved Area	Unpaved Area	Paved Area		
Catchment S1	-	-	0m²	2,114m²		
Catchment S2	20m <sup>2</sup>	245m <sup>2</sup>	0m²	265m <sup>2</sup>		
Catchment S3	148m²	197m²	0m²	345m <sup>2</sup>		
Catchment S4	56m <sup>2</sup>	119m²	0m²	175m <sup>2</sup>		
Catchment S5	16m <sup>2</sup>	214m²	0m²	230m <sup>2</sup>		
Catchment S6	122m <sup>2</sup>	49m²	0m²	171m²		
Catchment A1	3,274m <sup>2</sup>	446m²	3,274m <sup>2</sup>	446m²		
Catchment A2	2,828m <sup>2</sup>	253m <sup>2</sup>	2,828m <sup>2</sup>	253m <sup>2</sup>		
Catchment A3	1,854m²	361m <sup>2</sup>	1,854m²	361m <sup>2</sup>		
Catchment A4	974 m²	305m <sup>2</sup>	974m²	305m <sup>2</sup>		
Catchment A5	125 m <sup>2</sup>	225m <sup>2</sup>	125m <sup>2</sup>	225m <sup>2</sup>		
Catchment B	2,499m <sup>2</sup>	8,274m <sup>2</sup>	2,499m <sup>2</sup>	8,274m <sup>2</sup>		
Catchment C	23,853m <sup>2</sup>	15,231m <sup>2</sup>	23,853m <sup>2</sup>	15,231m <sup>2</sup>		
Catchment D	3,638m <sup>2</sup>	7,411m²	3,638m <sup>2</sup>	7,411m²		

\*Note: The runoff from Catchment S1 will be discharged to Stormwater Inlet Stormwater Inlet SIH1007504 via the existing village channel before Development.

## 2.7 ESTIMATED EXISTING AND FUTURE RUNOFF

## Peak Runoff to Box Culvert SBP1006180

- 2.7.1. Based on the changes of cumulative runoff shown in **Table 2.2**, the runoff at the Box Culvert SBP1006180 before and after the development was estimated based on the return periods of 50 years.
- 2.7.2. As shown in **Table 2.3** below, the estimated peak runoff discharged to the Box Culvert SBP1006180 before and after Development will be 2.551m³/s and 2.727m³/s respectively. There will be approximately 1.07 times increase in estimated peak runoff under the assessed return periods of 50 years. The detailed calculations of runoff discharge to Box Culvert SBP1006180 are provided in **Appendix C**.

Table 2.3 Estimated peak runoff discharge to Box Culvert SBP1006180

Return Period	E	Estimated Peak Runo	ff
	Before Development	After Development	% of Changes
50 Years	2.551m <sup>3</sup> /s	2.727m <sup>3</sup> /s	107%

<sup>\*</sup>Note: The runoff from Catchment S1 will be discharged to Stormwater Inlet SIH1007504 via the existing village channel before Development.

## Assessment of Drainage Capacity

2.7.3. As mentioned in Section 2.5.2, the runoff from the Project Site (Catchment S1) will be collected at the Proposed Terminal Manhole PTM1 and discharged to the Proposed Terminal Manhole PTM4 via the Proposed 375mm circular pipes. The runoff from the access road (Catchments S2 to S6) will be collected by the Proposed 600mm U-channels and discharged to the Proposed Terminal Manhole PTM4. All the runoff from the Application Site (Catchment S) will be discharged to the Box Culvert SBP1006180 via the Proposed 400mm circular pipes.

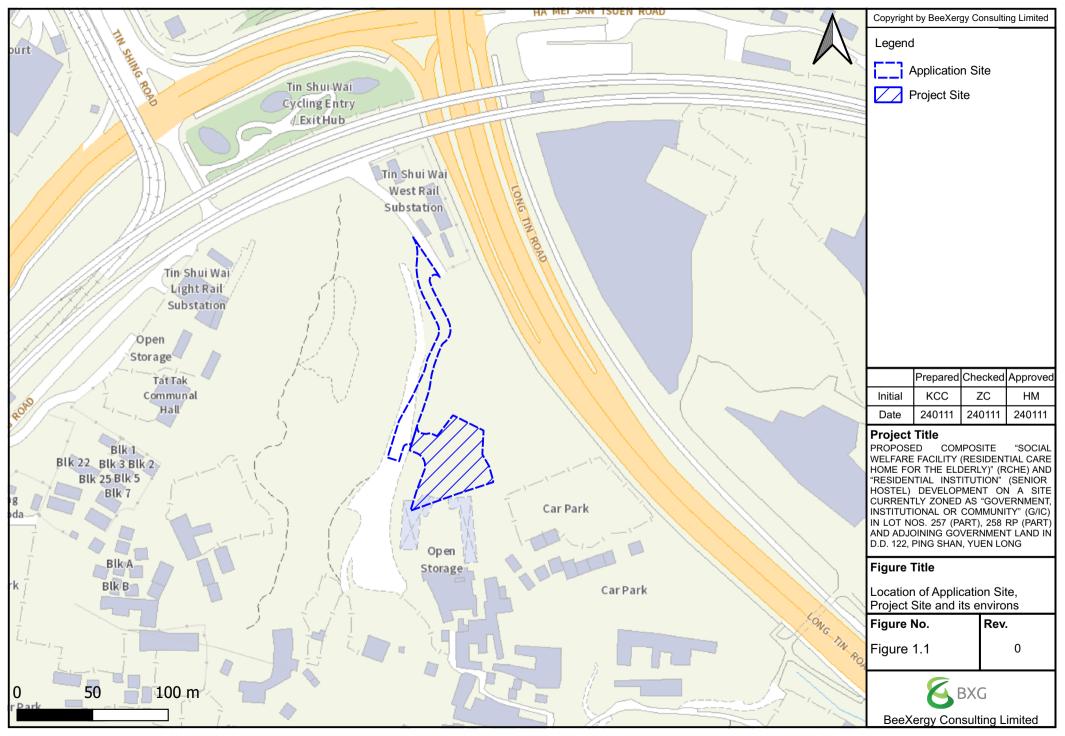
- 2.7.4. Calculation of drainage capacity of the runoff from the Project Site (Catchment S1) is provided in **Appendix D**.
- 2.7.5. Calculation of drainage capacity of the runoff from the access road (Catchments S2 to S6) and its associated upstream catchments (Catchments A1 to A5) is provided in Appendix E.
- 2.7.6. Calculation of drainage capacity of all runoff from the Application Site (Catchment S) and its associated upstream and downstream catchments (Catchments A, B, C, and D) is provided in **Appendix F**.
- 2.7.7. The results presented in **Appendices D**, **E**, and **F** suggested that the estimated peak runoff will not higher than 70% capacity of the drainage systems, and it is anticipated that the proposed drainage system will have sufficient capacity to cater to the surface runoff from the Proposed Development.
- 2.7.8. Given the runoff from the Application Site will no longer discharge via U-channel SUP1009961 and the existing village channel after Development, no additional runoff will be contributed to the U-channel SUP1009961 and the existing village channel, and adverse drainage impact is not anticipated.

## 3 CONCLUSION

- 3.1.1. The Project Proponent is proposed to develop a composite social welfare facility for Residential Care Home for the Elderly (RCHE) and residential institution for senior hostel at Lot Nos. 257 (Part), 258 RP (Part) and adjoining government land in D.D. 122, Ping Shan, Yuen Long.
- 3.1.2. Based on this DIA results, it is found that the proposed and existing drainage system serving the area has sufficient capacity to cater for the drainage generation from the Proposed Development and the surrounding catchment areas. Adverse drainage impact is not anticipated, and thus no upgrading or improvement works for existing drainage system are required.

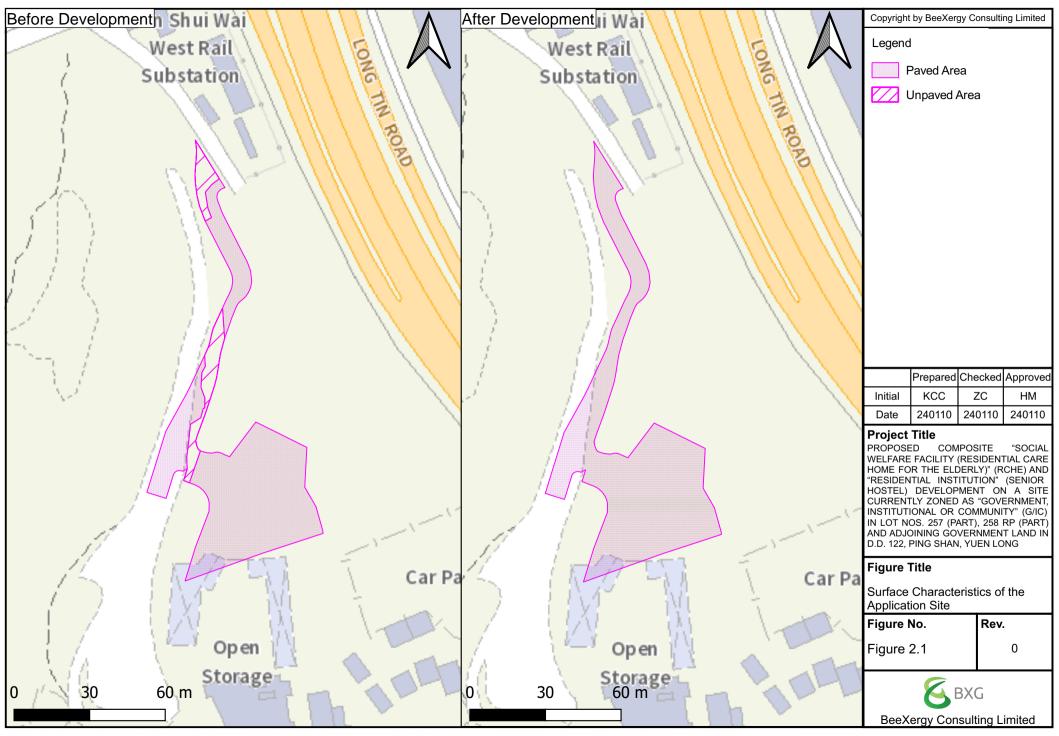


## FIGURE 1.1 LOCATION OF APPLICATION SITE, PROJECT SITE AND ITS ENVIRONS



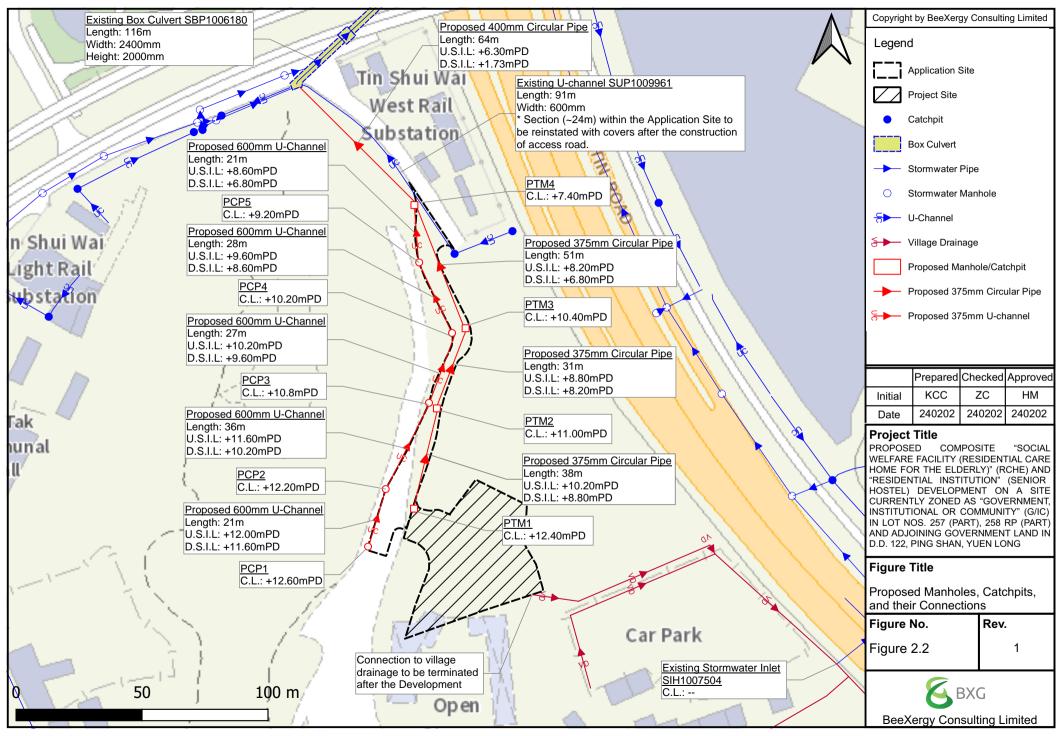


## FIGURE 2.1 SURFACE CHARACTERISTICS OF THE APPLICATION SITE



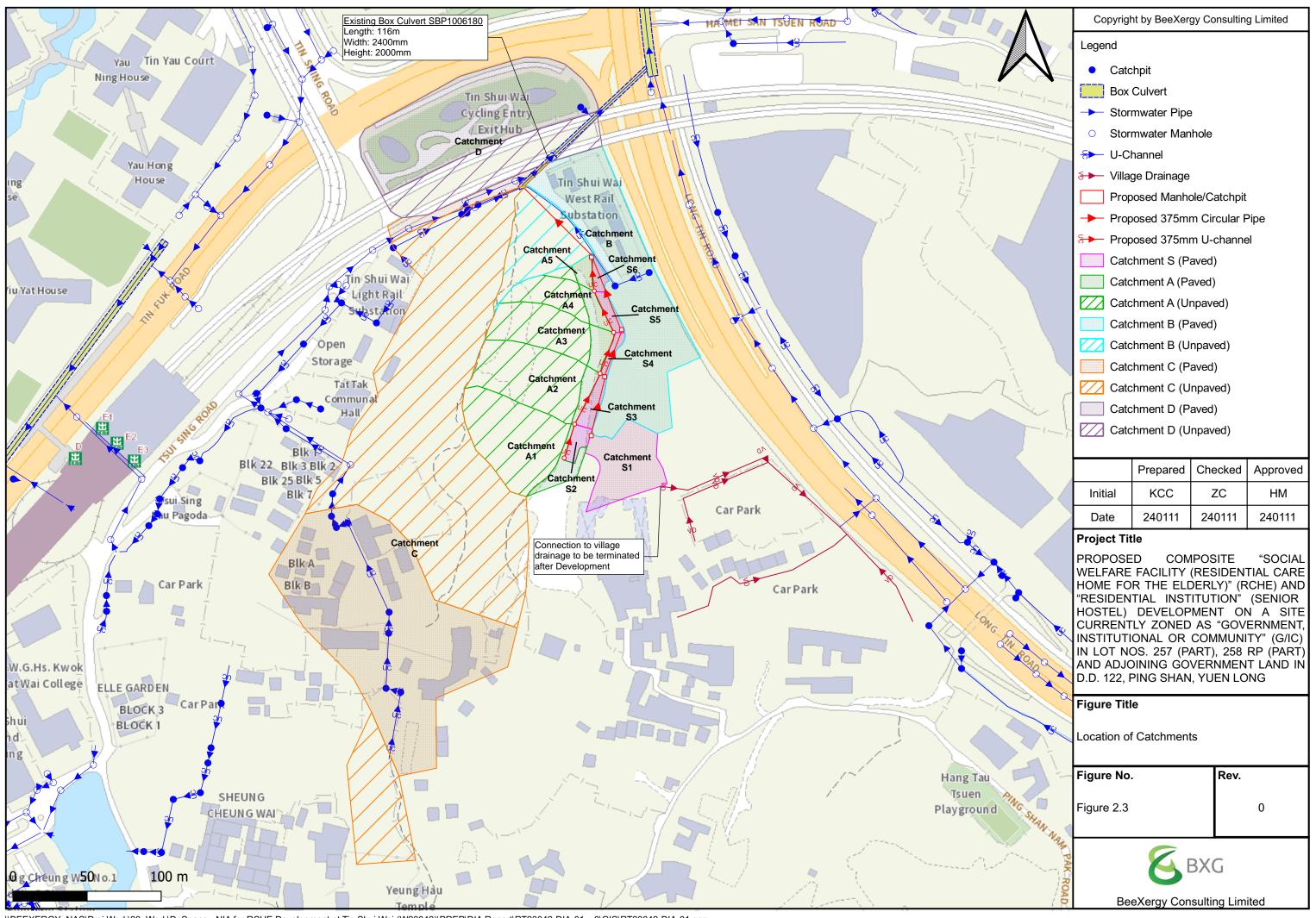


## FIGURE 2.2 PROPOSED MANHOLES, CATCHPITS AND ITS CONNECTIONS





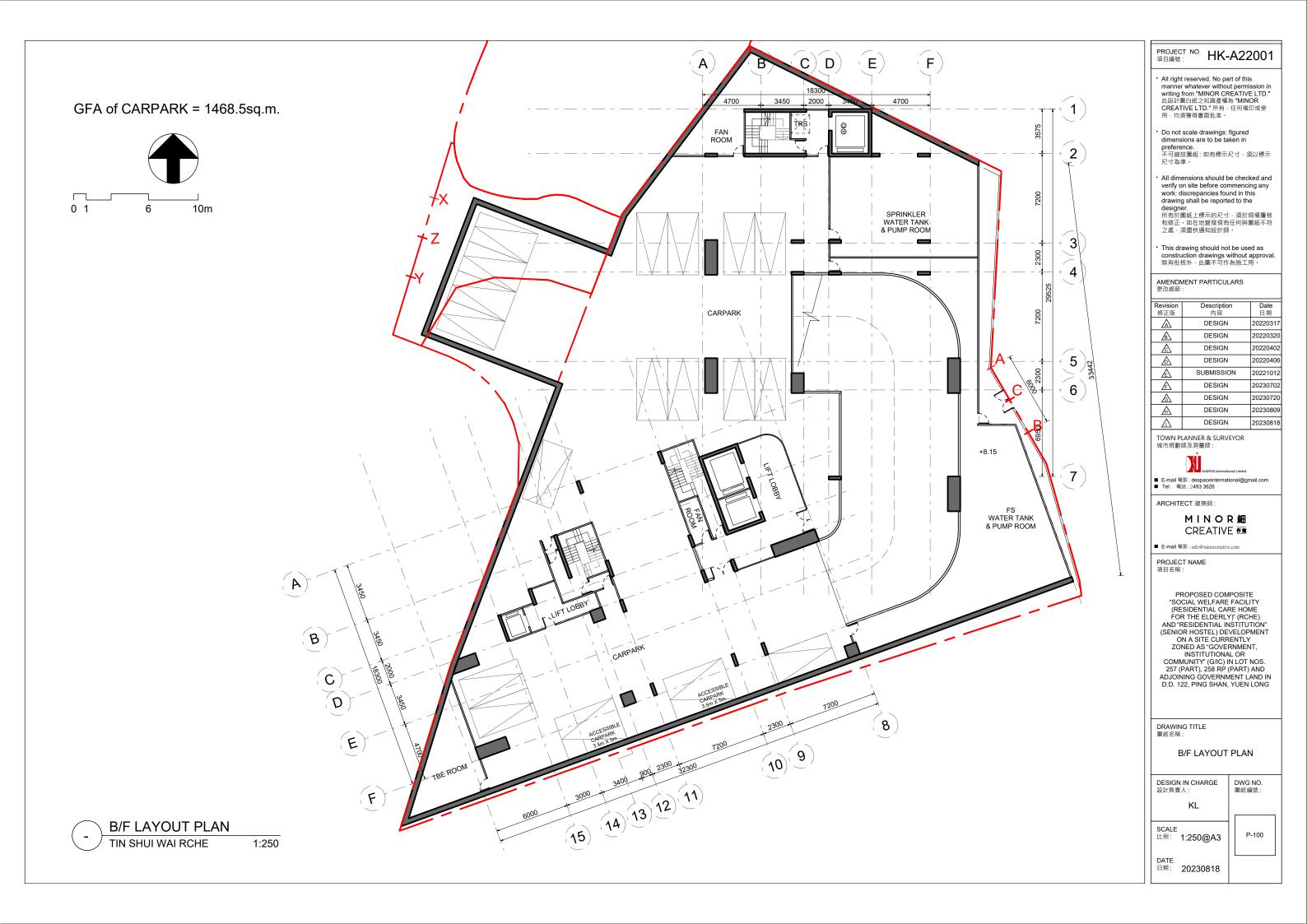
## FIGURE 2.3 LOCATION OF CATCHMENTS

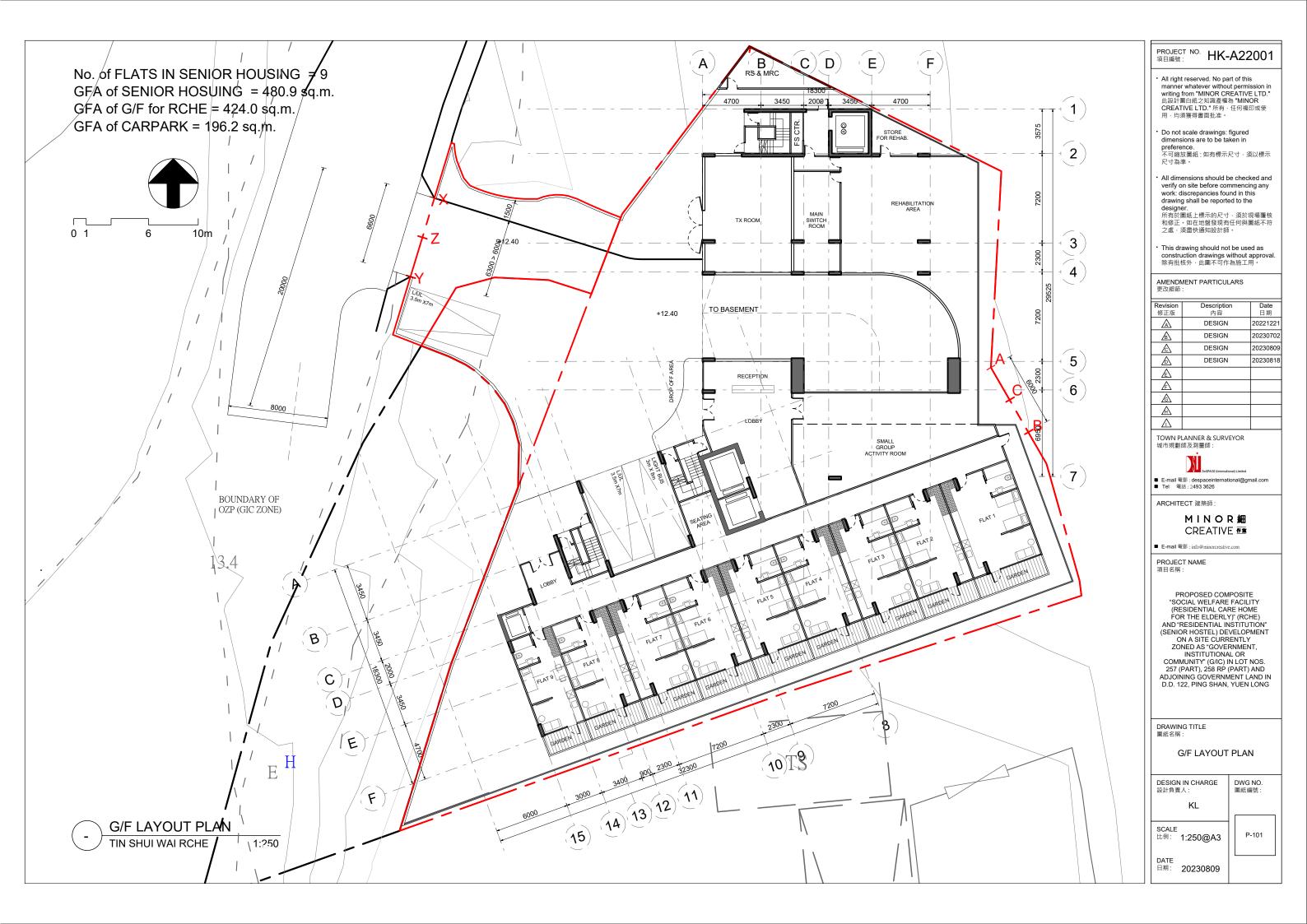




## APPENDIX A MASTER LAYOUT PLAN





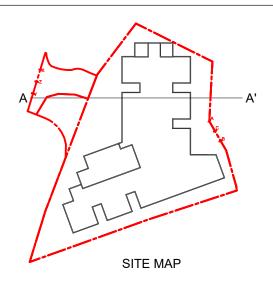


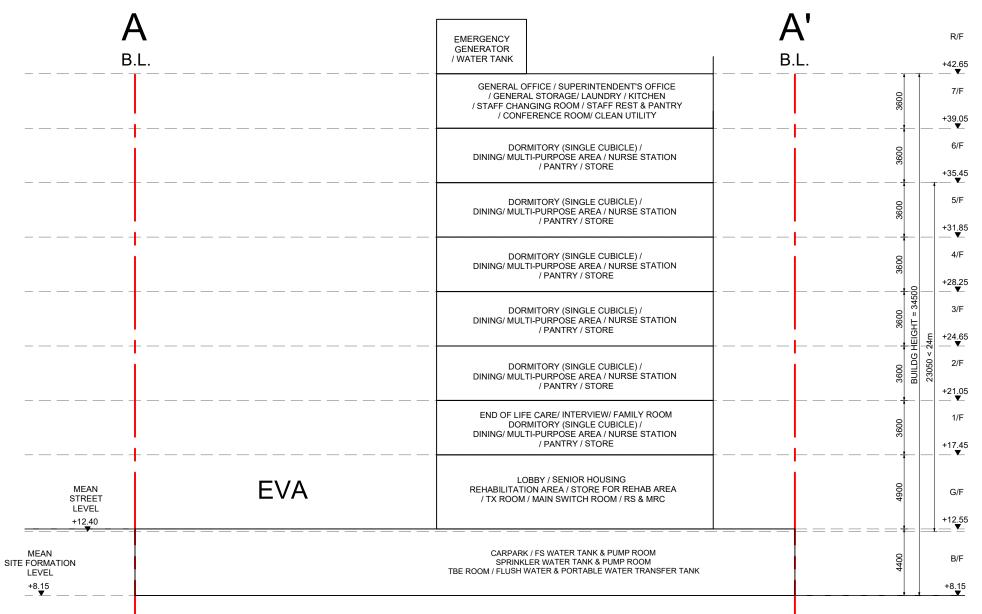












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## MINOR細 CREATIVE **6**

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PROJECT NAME

PROPOSED COMPOSITE
"SOCIAL WELFARE FACILITY
(RESIDENTIAL CARE HOME
FOR THE ELDERLY)" (RCHE)
AND "RESIDENTIAL INSTITUTION"
(SENIOR HOSTEL) DEVELOPMENT
ON A SITE CURRENTLY
TONED AS "TO VERMINENT" ZONED AS "GOVERNMENT, INSTITUTIONAL OR

COMMUNITY" (G/IC) IN LOT NOS. 257 (PART), 258 RP (PART) AND ADJOINING GOVERNMENT LAND IN D.D. 122, PING SHAN, YUEN LONG

DRAWING TITLE 圖紙名稱:

SCHEMATIC SECTION AA'

DESIGN IN CHARGE 設計負責人:

DWG NO.

S-101

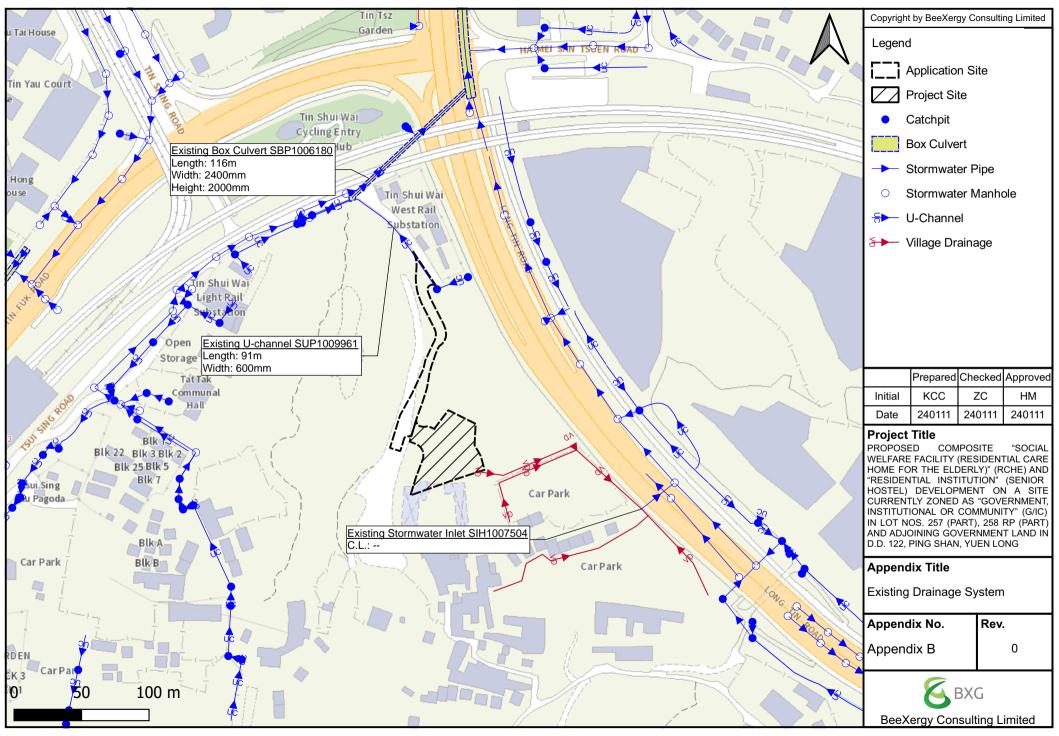
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## APPENDIX B EXISTING DRAINAGE SYSTEM





## APPENDIX C CALCULATION OF RUNOFF FOR RETURN PERIOD OF 50 YEARS

## Appendix C

## Calculation of Runoff for the Return Period of 50 Years

	Unpaved	Paved	Catchment Area Average clone Flow nath Inlet time (t.) Duration (t.)		Runoff intensity (i) with	Runoff coefficient for	Runoff coefficient for								
Catchment ID	Catchment Area (km²)	Catchment Area (km²)	(A), km <sup>2</sup>	(H), m/100m	length (L), m	min	min	а	b	С	climate change factor, mm/hr <sup>*</sup>	unpaved area (C <sub>up</sub> )	paved area (C <sub>p</sub> )	CxA	Peak runoff (Q <sub>p</sub> ) m <sup>3</sup> /s
Before the Proposed Development															
Catchment S1	0.000000	0.002114	0.002114	2.90	62	3.37	3.37	451.3	2.46	0.337	289.00	0.25	0.95	0.00201	0.161
Catchment S2	0.000020	0.000245	0.000265	1.15	26	2.09	2.09	451.3	2.46	0.337	314.13	0.25	0.95	0.00024	0.021
Catchment S3	0.000148	0.000197	0.000345	2.63	38	2.53	2.53	451.3	2.46	0.337	304.65	0.25	0.95	0.00022	0.019
Catchment S4	0.000056	0.000119	0.000175	3.55	31	2.08	2.08	451.3	2.46	0.337	314.49	0.25	0.95	0.00013	0.011
Catchment S5	0.000016	0.000214	0.000230	1.94	31	2.28	2.28	451.3	2.46	0.337	309.85	0.25	0.95	0.00021	0.018
Catchment S6	0.000122	0.000049	0.000171	7.41	27	1.56	1.56	451.3	2.46	0.337	327.44	0.25	0.95	0.00008	0.007
Catchment A1	0.003274	0.000446	0.003720	18.19	83	2.95	2.95	451.3	2.46	0.337	296.30	0.25	0.95	0.00124	0.102
Catchment A2	0.002828	0.000253	0.003081	22.32	82	2.85	2.85	451.3	2.46	0.337	298.15	0.25	0.95	0.00095	0.079
Catchment A3	0.001854	0.000361	0.002215	22.22	81	2.92	2.92	451.3	2.46	0.337	296.99	0.25	0.95	0.00081	0.067
Catchment A4	0.000974	0.000305	0.001279	22.41	58	2.20	2.20	451.3	2.46	0.337	311.60	0.25	0.95	0.00053	0.046
Catchment A5	0.000125	0.000225	0.000350	27.78	18	0.75	0.75	451.3	2.46	0.337	353.54	0.25	0.95	0.00025	0.024
Catchment B	0.002499	0.008274	0.010773	0.13	233	20.07	20.07	451.3	2.46	0.337	183.26	0.25	0.95	0.00849	0.432
Catchment C	0.023853	0.015231	0.039084	4.97	294	10.70	10.70	451.3	2.46	0.337	219.65	0.25	0.95	0.02043	1.248
Catchment D	0.003638	0.007411	0.011049	0.26	153	11.38	11.38	451.3	2.46	0.337	215.95	0.25	0.95	0.00795	0.477
														Total	2.712

	Unpaved	Paved	Catchment Area	Average slene	Flow path	Inlet time (t <sub>0</sub> ),	Duration (t <sub>d</sub> ),	Storm	n Const	ants <sup>*</sup>	Runoff intensity (i) with	Runoff coefficient for	Runoff coefficient for		
Catchment ID	Catchment Area (km²)	Catchment Area (km²)	(A), km²	(H), m/100m	length (L), m	min	min	а	b	С	climate change factor, mm/hr*	unpaved area (C <sub>up</sub> )	paved area (C <sub>p</sub> )	CxA	Peak runoff (Q <sub>p</sub> ) m <sup>3</sup> /s
After the Proposed Development															
Catchment S1	0.000000	0.002114	0.002114	0.97	62	4.20	4.20	451.3	2.46	0.337	276.35	0.25	0.95	0.00201	0.154
Catchment S2	0.000000	0.000265	0.000265	1.15	26	2.09	2.09	451.3	2.46	0.337	314.13	0.25	0.95	0.00025	0.022
Catchment S3	0.000000	0.000345	0.000345	2.63	38	2.53	2.53	451.3	2.46	0.337	304.65	0.25	0.95	0.00033	0.028
Catchment S4	0.000000	0.000175	0.000175	3.55	31	2.08	2.08	451.3	2.46	0.337	314.49	0.25	0.95	0.00017	0.015
Catchment S5	0.000000	0.000230	0.000230	1.94	31	2.28	2.28	451.3	2.46	0.337	309.85	0.25	0.95	0.00022	0.019
Catchment S6	0.000000	0.000171	0.000171	7.41	27	1.56	1.56	451.3	2.46	0.337	327.44	0.25	0.95	0.00016	0.015
Catchment A1	0.003274	0.000446	0.003720	18.19	83	2.95	2.95	451.3	2.46	0.337	296.30	0.25	0.95	0.00124	0.102
Catchment A2	0.002828	0.000253	0.003081	22.32	82	2.85	2.85	451.3	2.46	0.337	298.15	0.25	0.95	0.00095	0.079
Catchment A3	0.001854	0.000361	0.002215	22.22	81	2.92	2.92	451.3	2.46	0.337	296.99	0.25	0.95	0.00081	0.067
Catchment A4	0.000974	0.000305	0.001279	22.41	58	2.20	2.20	451.3	2.46	0.337	311.60	0.25	0.95	0.00053	0.046
Catchment A5	0.000125	0.000225	0.000350	27.78	18	0.75	0.75	451.3	2.46	0.337	353.54	0.25	0.95	0.00025	0.024
Catchment B	0.002499	0.008274	0.010773	0.13	233	20.07	20.07	451.3	2.46	0.337	183.26	0.25	0.95	0.00849	0.432
Catchment C	0.023853	0.015231	0.039084	4.97	294	10.70	10.70	451.3	2.46	0.337	219.65	0.25	0.95	0.02043	1.248
Catchment D	0.003638	0.007411	0.011049	0.26	153	11.38	11.38	451.3	2.46	0.337	215.95	0.25	0.95	0.00795	0.477
·														Total	2.727

### Remark

The runoff from Catchment S1 will be discharged to Stormwater Inlet Stormwater Inlet SIH1007504 via the existing village channel before the Proposed Development. The runoff from Catchment S2-S6, A1-A5, B, C, and D will be discharged to Box Culvert SBP1002932 via the U-channel SUP1009961 before the Proposed Development. All runoff will be discharged to Box Culvert SBP1002932 via proposed connection after the Proposed Development.

According to SDM Table 3a and Figure 3, the storm constants for the return period of 50 years of the HKO Headquarters will be 451.3 (a), 2.46 (b), and 0.337 (c).

According to Stormwater Drainage Manual CORRIGENDUM No. 1/2022 - Table 28, the rainfall increases due to Climate Change will be 16.0% for end of 21st Century.



# APPENDIX D CALCULATION OF DRAINAGE CAPACITY OF THE RUNOFF FROM THE PROJECT SITE (CATCHMENT S1)

## Appendix D

## Calculation of drainage capacity of the runoff from the Project Site (Catchment S1)

SECT	TION	Pipe	Catchment	Length	Upstream Invert Level	Downstream Invert Level	d	r	A <sub>w</sub>	P <sub>w</sub>	R	s	k <sub>s</sub>	v	Q <sub>c</sub>	Total Runoff in 50 Years	% of capacity	Remark
From	То			m	mPD	mPD	m	m	m <sup>2</sup>	m	m	-	mm	m/s	m³/s	m³/s	%	
PTM1	PTM2	1 x 375mm circular pipe	\$1	38	+10.20	+8.80	0.375	0.19	0.110	1.178	0.09	0.037	0.06	4.4269	0.489	0.154	32%	OK
PTM2	PTM3	1 x 375mm circular pipe	\$1	31	+8.80	+8.20	0.375	0.19	0.110	1.178	0.09	0.019	0.06	3.1814	0.351	0.154	44%	OK
PTM3	PTM4	1 x 375mm circular pipe	\$1	51	+8.20	+6.80	0.375	0.19	0.110	1.178	0.09	0.027	0.06	3.8074	0.421	0.154	37%	ОК

## Legend

d = pipe diameter, m

r = pipe radius (m) = 0.5d

 $A_w$  = wetted area (m<sup>2</sup>) =  $\pi r^2$  (circular) ;  $\pi r^2/2$  (U-channel) ; WH (Box Culvert)

 $P_w$  = wetted perimeter (m) =  $2\pi r$  (circular);  $\pi r$  (U-channel); 2W+2H (Box Culvert)

 $R = Hydraulic radius (m) = A_w / P_w$ 

s = Slope of the total energy line

k<sub>s</sub> = equivalent sand roughness, mm

V = Velocity of flow calculated based on Colebrook White Equation, m/s

Q<sub>c</sub> = Flow Capacity (10% sedimentation incorporated), m<sup>3</sup>/s

Q<sub>p</sub> = Estimated total peak flow from the Site during peak season, m<sup>3</sup>/s



## **APPENDIX E**

CALCULATION OF DRAINAGE CAPACITY OF THE RUNOFF FROM THE ACCESS ROAD (CATCHMENTS S2 TO S6) AND ITS ASSOCIATED UPSTREAM CATCHMENTS (CATCHMENTS A1 TO A5)

## Appendix E

Calculation of drainage capacity of the runoff from the access road (Catchments S2 to S6) and its associated upstream catchments (Catchments A1 to A5)

SEC	TION	Pipe	Catchment	Length	Upstream Invert Level	Downstream Invert Level	d	r	A <sub>w</sub>	P <sub>w</sub>	R	s	k <sub>s</sub>	v	Q <sub>c</sub>	Total Runoff in 50 Years	% of capacity	Remark
From	То			m	mPD	mPD	m	m	m <sup>2</sup>	m	m	-	mm	m/s	m³/s	m³/s	%	
PCP1	PCP2	1 x 600mm U-channel	\$2+A1	21	+12.00	+11.60	0.600	0.30	0.141	0.942	0.15	0.019	0.06	4.2104	0.595	0.124	21%	OK
PCP2	РСР3	1 x 600mm U-channel	S2+S3+A1+A2	36	+11.60	+10.20	0.600	0.30	0.141	0.942	0.15	0.039	0.06	6.0611	0.857	0.231	27%	OK
PCP3	PCP4	1 x 600mm U-channel	S2+S3+S4+A1+A2+A3	27	+10.20	+9.60	0.600	0.30	0.141	0.942	0.15	0.022	0.06	4.5559	0.644	0.312	48%	OK
PCP4	PCP5	1 x 600mm U-channel	S2+S3+S4+S5+A1+A2+ A3+A4	28	+9.60	+8.60	0.600	0.30	0.141	0.942	0.15	0.036	0.06	5.8040	0.821	0.377	46%	OK
PCP5	PTM4	1 x 600mm U-channel	S2+S3+S4+S5+S6+A1+ A2+A3+A4+A5	21	+8.60	+6.80	0.600	0.30	0.141	0.942	0.15	0.086	0.06	9.0530	1.280	0.416	32%	OK

## Legend

d = pipe diameter, m

r = pipe radius (m) = 0.5d

 $A_w$  = wetted area (m<sup>2</sup>) =  $\pi r^2$  (circular) ;  $\pi r^2/2$  (U-channel) ; WH (Box Culvert)

 $P_w$  = wetted perimeter (m) =  $2\pi r$  (circular) ;  $\pi r$  (U-channel) ; 2W+2H (Box Culvert)

R = Hydraulic radius (m) = A<sub>w</sub> / P<sub>w</sub>

s = Slope of the total energy line

k<sub>s</sub> = equivalent sand roughness, mm

V = Velocity of flow calculated based on Colebrook White Equation, m/s

Q<sub>c</sub> = Flow Capacity (10% sedimentation incorporated), m<sup>3</sup>/s

Q<sub>p</sub> = Estimated total peak flow from the Site during peak season, m<sup>3</sup>/s



## **APPENDIX F**

CALCULATION OF DRAINAGE CAPACITY OF ALL RUNOFF FROM THE APPLICATION SITE (CATCHMENT S) AND ITS ASSOCIATED UPSTREAM AND DOWNSTREAM CATCHMENTS (CATCHMENTS A, B, C, AND D)

## Appendix F

Calculation of drainage capacity of all runoff from the Application Site (Catchment S) and its associated upstream and downstream catchments (Catchments A, B, C, and D)

SECTION		Pipe	Catchment	Length	Upstream Invert Level	. d r	r	A <sub>w</sub>	P <sub>w</sub>	R	s	ks	v	Q,	Total Runoff in 50 Years	% of capacity	ty Remark	
From	То			m	mPD	mPD	m	m	m²	m	m	-	mm	m/s	m³/s	m³/s	%	
PTM4	Box Culvert SBP1006180	1 x 400mm circular pipe	S + A	64	6.30	1.73	0.400	0.20	0.126	1.257	0.10	0.071	0.06	6.4464	0.810	0.570	70%	ОК
Box Culvert SBP1006180	Box Culvert SBP1002932	2400mm x 2000mm Box Culvert	S+A+B+C+D	116	1.73	1.51	2.400	1.20	4.800	8.800	0.55	0.002	0.06	2.8191	13.532	2.727	20%	ОК

## Legend

d = pipe diameter, m

r = pipe radius (m) = 0.5d

 $A_w$  = wetted area (m<sup>2</sup>) =  $\pi r^2$  (circular);  $\pi r^2/2$  (U-channel); WH (Box Culvert)

 $P_w$  = wetted perimeter (m) =  $2\pi r$  (circular);  $\pi r$  (U-channel); 2W+2H (Box Culvert)

R = Hydraulic radius (m) = Aw / Pw

s = Slope of the total energy line

k<sub>s</sub> = equivalent sand roughness, mm

V = Velocity of flow calculated based on Colebrook White Equation, m/s

Q<sub>c</sub> = Flow Capacity (10% sedimentation incorporated), m<sup>3</sup>/s

Q<sub>p</sub> = Estimated total peak flow from the Site during peak season, m<sup>3</sup>/s

### Remark:

(1) The upstream invert level and downstream invert level of Box Culvert are referenced from the downstream invert level of SWD1059683 and SWD1034861 respectively.