# DRAINAGE IMPACT ASSESSMENT & DRAINAGE PROPOSAL

PROPOSED TEMPORARY OPEN STORAGE OF CONSTRUCTION MATERIALS FOR A PERIOD OF 3 YEARS LOT 137(PART) IN DD128, HA TSUEN, YUEN LONG

APT ARCHITECTS LIMITED

#### PROPOSED TEMPORARY OPEN STORAGE OF CONSTRUCTION MATERIALS LOT 137(PART) IN DD128, HA TSUEN, YUEN LONG REVISED DRAINAGE IMPACT ASSESSMENT AND PROPOSAL

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#### PROPOSED TEMPORARY OPEN STORAGE OF CONSTRUCTION MATERIALS LOT 137(PART) IN DD128, HA TSUEN, YUEN LONG REVISED DRAINAGE IMPACT ASSESSMENT AND PROPOSAL

#### 1.0 INTRODUCTION

1.1 This report is a drainage proposal for the Following Sites in Ha Tsuen, Yuen Long:

Site Area 510m2 (about) Lot 137 (part) in DD128

1.2 The proposed use of the site is **Temporary Open Storage of Construction Materials** for a Period of 3 Years.

#### 2.0 THE DRAINAGE PROPOSAL

2.1 The **Condition** of the **Application Site** is as follows:

Main access of the Site is through local village road from Fung Kong Tsuen Road.

The Application SITE is paved with concrete and formed levelled with fall towards North-West. Gradient of Site is greater than 1:200.

The Site is adjacent to two Sites with the following Town Planning Application Ref:

A/YL-HTF/1119, **Catchment CA**, which is adjacent to APPLICATION SITE, at downstream, Area about 725m2 A/YL-HTF/1134, **Catchement CA1+CA2**, which is at west side of APPLICATION SITE

<u>The Site is formed higher than adjacent access road</u> (to the east of SITE / CA), therefore runoff of CA3 will not affect Application SITE and the downstream site CA.

Part of Runoff of Catchment CA4 will affect the SITE, will be handled by D11.

Revised DRAINAGE PROPOSAL plan no. D-01 (J1) is enclosed. Please refer to Response to Comments below.

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#### 2.2 DRAINAGE SCHEDULE of the Application Site and Downstream Drains :

No.	Size in mm, fall	Remarks
G1	300x300 with Metal Grating,	at entrance of SITE; higher than
	min 1:100	surrounding lands and road;
		discharge only to D13, via CP12 at corner
D11	400x400 min 1:70	at upper part of Site, will collect 10% of
		runoff of CA4 (part of CA3)
		*remaining CA4 discharge towards
		west/north west, to be collected by lower
		channels of other sites, D3,D3A,D6,D7,D9
D12	400x400 min 1:30	take 30% SITE RUNOFF
D13	400x400 min 1:50	take 70% SITE RUNOFF;
CP13	Catchpit min 400D, Last Manhole of	TAKE 100% SITE RUNOFF,
	SITE	discharge to D22

<u>The whole Site is levelled higher than access Road to the east</u>, therefore the Site peripheral U-channel will not be affected by adjacent lands / access road; <u>Only minor runoff of Catchment CA4 (10%) will be handled by D11.</u>

Accordingly all discharge from SITE is handled by D12, D13 and collected to CP13, then discharge to drain channel D22 (shared with neighbour Site).

As Application Site is small, D13 discharing to CP13, and this catchpit is shared by lower Site CA (of A/YL/HTF/1119). In case site level of CP13 serving both Site has other factors, CP13 will split into 2, one for Application Site, and one for lower Site CA.

#### 2.3 **DOWNSTREAM DRAINAGE FACILITIES** to be used by Application Site:

#### 2.3a CA (drain channels handle 100% runoff from APPLICATION SITE)

Peripheral U-Channel of minimum 1:200 fall of size 400mm x 400mm is proposed for the entire Site CA.

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D13 is shared by two sites (application SITE + CA); while D13 is of upstream of CA, will handle about 10% of runoff of CA.

CA is also formed higher than road of east side, and is of about 1.2m lower than Application Site.

D22 will handle all from Site A, and 50% runoff of Site B.

2.3b **Application Site** and **CA** runoff will be collected in CP15 and discharge to CP2 via D25 (400X400), and **WILL USE facilities of Site C** (CA1+CA2).

All runoff will be discharge ultimately to drainage at public areas via **D6**, **D7**, and **D9** finally to existing **open village channel DD**, where it is discharged via existing underground pipe to north-west across the road to downstream public drainage network.

2.4 **Hydraulic Calculation** (attached) shows that the capacity of all downstream drains D6, D7, are adequate for the runoff of **Site** + Site CA + Site C (CA1+CA2), and has also checked neighbouring capacity of CA3, CA4, and CA5.

#### **3.0 RESPONSE TO COMMENTS** (i-viii to corresponds to DSD's comments of 28/07/2023)

- i. **Drawing D-01 (rev J1)** Proposed U Channels D13 and D13A will separately serve **Application Site** and **lower Site CA** (A/YL-HTF-1119) ; and will be collected at catchpit CP13 (shared by both sites).
- ii. Most runoff from CA4 is to be handled by D11, D3, D3A, D6, D7, D8 and D9; the percentage is for arithmetical / geometric share (refer D-02 Flow Pattern Plan) of runoff to these channels, and <u>each of these channels are having spare capacity to handle spare percentage runoff by calculation</u>.
- iii Please refer to Revised Hydraulic Calculation for each channel.
- iv. The Application Site is formed higher than the road serving the Site, and Site is designed to fall away from G1; accordingly G1, will only have minimal runoff to handle.

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v. discrepancy between plan and calculation were updated;

vi. DD - photo has demonstrated it's presence; please also note that the CP10 has been updated on Plan to tally with existing site condition (refer to photo below);

vii. refer photo below, and path from D6 to D9, and CP10 – DD, all to be constructed;

viii. CP10 is the last manhole before discharging to DD (the undergound pipe).



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#### 3.1 CONSTRUCTION & MAINTENANCE OF PROPOSED DRAINAGE

- The applicant of the Application SITE A (Application Site), related neighbour Sites (CA, CA1+CA2) will all undertake to construct and to be responsible for the maintenance works for the proposed drainage system being constructed (D6 / D7 and related Catchpits) at their own costs.
- b. Lowest common Drainage D7 (lower portion) and D9, is to be constructed by Applicant of other Site (ref: A/YL-HTF/1111). The DIA of this Site (plan attached per Appendix) was approved by PlanD/DSD in 2022. We also enclose consent letter per Appendix between Site at west (CA1+CA2) and Site CA5A for arrangement of construction of the said lowest common drain (D7/D9).
- c. Inspection, cleansing and desilting will be carried out regularly and before / after the rainy season each year to ensure the drainage facilities functions efficiently. Since the system is designed to operate under gravity, the maintenance will be straightforward.

#### 4.0 CONCLUSION

4.1 This drainage impact assessment is primarily based on site condition and existing / newly constructed drainage system at downstream of the said SITE(s). The stormwater drainage system is in a simple manner and is of adequate spare capacity without jeopardizing the neighboring areas and environment.

The development will not obstruct overland flow nor adversely affect existing village drains of the adjacent areas. And that the Site has not affect the natural fall manner of the peripheral areas, and that capacity of the Drainage system has also take into consideration the possible discharge from the neighbour.

All assumptions made were on conservative side of uniform flow in size and gradient.

4.2 From this assessment, it can be concluded that the proposed drainage will have no adverse impacts to the site and it has also maintain a good balance to the possible discharge from surrounding sites and other upstream areas.









Runoff Coefficient		Manning Coefficient					
crush stone and asphalt	0.7	Conc/Cement	0.013				
grassland	0.25	Steel, PVC	0.011				
concrete	1	dredged	0.03				

#### DRAINAGE PROPOSAL - HYDRAULIC CALCULATION

LOT 137 (PART) OF DD128, HA TSUEN, YUEN LONG (v23.09)

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Catchment Area	CA1	CA2	APPLICATION SITE	CA	CA3	CA4		CA5
	(SITE at west)	SITE at west		(downstream site)				
					Partly paved,			
					Grassland, Crush	Partly paved/Crush		Partly paved/Crush
Ceiling / Paving Material	Concrete paving	Concrete paving	Concrete paving	Concrete paving	stone	Stoe		Stoe
C = Runoff Coefficient	1	1	1	1	0.75	0.75		0.75
Area (m2)	1280	1820	510	725	7500	34000		15000
A = Area (km2)	0.00128	0.00182	0.00051	0.000725	0.0075	0.034		0.015
L = site length (m)	45	70	45		30	300		180
Top Level	24.1	23.8	28.6	27.9	33	33		22
Low Level	23.4	21.7	27.5	26.2	21.0	10.8		10.8
H = Average slope (m per 100m)	1.56	3.00	2.44		160.00	7.40		6.22
to = Time of Conc (min.)	11.599	15.275	11.618	11.667	2.565	40.780		27.491
i (mm/h)	215.540	197.413	215.432	215.154	307.780	138.896		160.903
Qp Peak Run off (m3/s)	0.0767	0.0999	0.0305	0.0434	0.4813	0.9846		0.5032
Note: other runoff	to add 10% of CA3	to add 20% of CA3						
(m3/s)	0.048	0.096	0.031	0.043				

	D2 (entrance)	D1	D1A	D3	D3A	D6	D7	D8	D9	) DD		D5	D11	D12	D13	D22	D23	D25
											1		Rect. U-	Rect. U-	Rect. U-	Rect. U-	Rect. U-	
Shape	Rectangular U-channel	Rect. U-channel	Rect. U-channel	Rect. U-channel	Rect. U-channel	Rect. U-channel	Rect. U-channel	Rect. U-channel	Rect. U-channe	CIRCLULAF	R	CIRCULAR	channe	l channel	channe	channel	channe	CIRCULAR
Material	cement	cement	cement	cement	cement	cement	cement			CONCRETE	-	PVC	cement	cement	cement	cement	cement	PVC
Mann Coeff	0.013	0.013	0.013	0.013	0.013	0.013	0.013	0.013	0.013	3 0.013	3	0.011	0.013	0.013	0.013	0.013	0.013	0.011
width	0.45	0.45	0.45	0.45	0.45	0.60	0.60	0.75	1.50	0.90	diameter	0.60	0.40	0.40	0.40	0.40	0.40	0.60
depth	0.45	0.45	0.45	0.45	0.45	0.60	0.60	0.75	0.70				0.40	0.40	0.40	0.40	0.40	
	(u-channel)		(u-channel)	(u-channel)	(u-channel)	(u-channel)	(u-channel)	(u-channel)	(u-channel	) CONCRETE U/G PIPE	Ξ	PVC PIPE	(u-channel)	(u-channel)	(u-channel)	(u-channel)	(u-channel)	PVC PIPE
		50.0						25.0									50.0	
Length	24.0	50.0	60.0	38.0	38.0	30.0	35.0	25.0	90.0	125.0	Length	1.0	40.0	14.0	40.0	30.0	50.0	2.0
l op Level (start)	22.00	23.70	23.40	23.70	22.40	17.80	16.20	11.63	11.25	9.60	Top Level (start)	20.90	28.40	27.80	28.00	27.20	27.50	25.40
Low Level (end)	21.70	23.40	22.40	22.40	20.90	16.20	11.63	11.25	9.60	5.80	Low Level (end)	18.40	27.80	27.20	27.20	25.40	25.40	23.80
	0.30	0.30	1.00	1.30	1.50	1.60	4.57	0.38	1.0		St, Slope =	2.50	0.60	0.60	0.80	1.80	2.10	0.80
SI, Slope =	0.01250	0.00600	0.01667	0.03421	0.03947	0.05333	0.13057	0.01520	0.01833	0.02240	Slope (1 to ?)	section letters	0.01500	0.04286	0.02000	0.06000	0.04200	
Slope (1 to ?)	80	167	60	35	35	19	8	66	5	45		vertical pipe	6/	23	50	1/	24	vertical pipe
A, Area = u channel by CAD	0.20	0.20	0.20	0.20	0.20	0.36	0.36	0.56	1.05	5 0.64	A, Area =	0.28	0.16	0.16	0.16	0.16	0.16	0.28
P, perimeter = u channel	1.35	1.35	1.35	1.35	1.35	1.80	1.80	2.25	3.70	0.26	Mean Depth	0.17	1.20	1.20	1.20	1.20	1.20	0.17
R = A/P =	0.15000	0.15000	0.15000	0.15000	0.15000	0.20000	0.20000	0.25000	0.28378	3	R = A/P =		0.13333	0.13333	0.13333	0.13333	0.13333	
$V_{\rm r}$ Valacity = $P1/6/(P(f)1/2)$	2 420	1 600	2 804	4.017	4 215	6.075	0 506	2 764	4.400	52 600		44.002	2.450	4 156	2 020	4 019	1 1 1 1	25.401
(1)	0.492	0.3/1	0.568	4.017	4.313	2 187	3.300	3.704 2 117	4.430	32.050	v, velocity	12 696	0 393	4.150	0.454	4.518	0.658	7 182
	0.432	0.341	(for D3, D5 similar)	0.015	0.074	2.107	5.422	2.117	4.72	55.520	Capacity -AV (110/3	12.050	0.353	0.005	0.454	0.707	0.050	7.102
	MAY 25% of CA2 +	MAY 25% of CA2+	taka 50% CA1	taka 50% CA1	tako all D1A	take all of CA1+CA2	take 60% CA2 (incl Site	take 60% CA2 (incl Site	take 60% CA2 (incl Site			take all of		TAKE 30% OF	TAKE 70% OF	TAKE 50% CA	TAKE 50% CA	ΤΔΚΕ ΔΙΙ
	WIAA.2370 01 CAS +	WIAA 25% OF CAS+	ALL OF APPLICATION SITE + SITE CA	lake 50% CAL,	D3+40%CA2		A + Site B)	A + Site B)	A + Site B	1.4309, compare with capcity of DD=	- h =	CA1+CA2, and	CA4 RUNOFF	SITE RUNOFF	SITE RUNOFF	RUNOFF , all of SITE A	RUNOFF	SITE A+ SITE B RUNOFF
	20% of CA2 (lower site)	20% of CA1	& 10% of CA4	& TOTAL 20% of CA4 )	& extra10% of CA4	& S1 + 50% of CA4(upper)	+50%CA4 +70%CA5	+60%CA4 +80%CA5	+70%CA4 5 +90%CA	4 33.5200 5	D	40% CA3 + 40% CA4		+runoff of D11		incl 20% of CA4		incl 10% of CA4
TOTAL RUNOFF TO HANDLE	0.1403	0.1357	0.3134	0.2353	0.6871	0.8438	1.1333	1.2821	1.4309	9 1.4309	9	0.7148	0.0985	0.1076	0.0214	0.1507	0.0217	0.1724
	<0.492 OK	<0.249 OK	<0.568 OK	<0.813 OK	<0.874 OK	<2.187 OK	<3.422 OK	<2.117 OK	<4.723	3 <33.52	2	<12.696 OK	<0.393 OK	<0.665 OK	<0.454 OK	<0.787 OK	<0.658 OK	<7.182 OK

D9 RUNOFF OF ALL SURROUNDING LAND ONLY OCCUPIES MINIMAL CAPACITY OF DD

COMMENTS FROM CALCULATION

1. APPLICATION SITE (THIS APPLICATION), 400X400MM IS ADEQUATE TO HANDLE SITE RUNOFF; SITE IS LEVELLED HIGHER THAN ADJACENT ROAD, AND 20% RUNOFF FROM UPSTREAM (CA4)

2A. NEIGHBOUR (LOWER) SITE CA, D22 400X400MM IS ADEQUATE TO HANDLE RUNOFF FROM APPLICATION SITE , and 10% OF CA4

2B. NEIBHBOUR SITE (CA1+CA2), D2, D4 IS ADEQUATE TO HANDLE RUNOFF FROM BOTH APPLICATION SITE, AND SITE CA

3. CATCHMENT CA4 INCLUDES ALL DOWNSTREAM FACILITIES FOR APPLICATION SITE AND SITE CA, D7, D8, D9 CAN HANDLE ACCUMULATED CAPACITY OF UP TO 60% RUNOFF OF CA3, 70% OF CA4 AND 90% FROM CA5

4. CAPACITY OF EXISTING PUBLIC U/G CHANNEL DD OF 0.9M DIAMETER, IS ADEQUATE TO HANDLE ACCUMULATED RUNOFF OF D9

#### **APPLICATION SITE**



敬啟者

鍾柏祥先生為規劃申請編號: A/YL-HTF/1111的申請者·申請地點為新界元朗厦村丈量約份第128約地段第134號(部分)、第159號餘段(部分)、第161號(部分)、第162號(部分)、第 163號B分段(部分)及第173號(部分)及毗連政府土地·用途作為期三年的臨時露天存放五金。

卓滙香港發展有限公司為規劃申請編號: A/YL-HTF/1149的申請者,申請地點為新界 元朗厦村丈量約份第 128 約地段第136 號(部分)、第141號(部分)及第142號(部分)和毗連政府 土地,用途作為期三年的臨時露天存放五金廢料及物流中心連附屬辦公室。

附圖一·為規劃申請: A/YL-HTF/1111的排水渠走向,於2022年獲渠務署接納。其排 水走向有部分與A/YL-HTF/1149的排水渠走向(即附圖二)相同,出現重疊的情況。鍾先生及 卓滙香港發展有限公司經商議後,鍾先生會先落實排水渠,有關部分重疊的排水渠亦會由鍾先 生落實。日後,對於部分重疊的排水渠,卓滙香港發展有限公司願意使用鍾先生即 A/YL-HTF/1111所擬議並落實的排水渠。鍾先生亦歡迎鄰近的場地經營者使用部分重疊的排水 渠,包括A/YL-HTF/1149的申請人。



(附圖一: A/YL-HTF/1111的排水渠走向)



(附圖二: A/YL-HTF/1149的排水渠走向)

此致

+6

城規會 / 規劃署 / 渠務署

Ching kul i

鍾柏祥先生



卓滙香港發展有限公司

## 2023年04月30日











