

Appendix 4.6b

Detailed Calculation of In-Tunnel Air Quality
for the Short Section of the Underpass

Tunnel Parameter

One way, One lane		
Length L	=	48 m
Height H	=	9 m
Width W	=	8 m
Cross-sectional area $A_T = H \times W$	=	72 m ²
Perimeter P	=	34 m

Emission Data

Traffic flow = 627 veh/hr

Traffic Breakdown % vehicle	M/C	Car/Taxi	Minibus	LGV	HGV	Bus
	3	67	6	11	5	8
NO _x Emission Factor (EURO 3)	0.46	0.8	1.67	1.35	4.67	8.44 g/km

Total NO_x emission factor = 1.707 g/km/veh

Total NO₂ emission rate = total NO_x emission factor x traffic flow x tunnel length x NO₂ conversion factor
where conversion factor = 12.5% (including tailpipe NO₂ emission taken as 7.5%
of NO_x and 5% of NO₂/NO_x for tunnel air)
= 0.001784 g/sec

Vehicle Data

Nominal dimensions of vehicles are given in Transport Planning and Design Manual, Vol. 2 as:

	W /m	H /m	L /m
Cars and Taxi	1.7	1.5	4.6
Light Bus	2	3	6.5
LGV	2.1	1.6	5.2
HGV	2.5	4.6	16
Bus	2.5	4.6	12

* No dimensions for motor cycle are provided.

* For the purpose of this study, the dimensions of motor cycle are assumed to be the same as private car.

$$\text{Nominal cross-sectional area } A_C = (0.03+0.67)*1.7*1.5+0.06*2*3+0.11*2.1*1.6+(0.05+0.08)*2.5*4.6$$

$$= 4.0096 \text{ m}^2$$

Tunnel Airflow

For Uni-directional Traffic,

Push Force by vehicles:

$$F_C = \frac{1}{2} \rho (V_C - V_T)^2 C_d A_C N$$

Resisting Force by tunnel:

$$F_T = \frac{1}{2} \rho V_T^2 (K_{in} + K_{out} + \frac{fL}{D}) A_T$$

External Wind at the Entrance and Exit Portals:

$$F_W = \frac{1}{2} \rho C_w (V_W \cos \theta)^2 A_T$$

where ρ = Air density = 1.2 kg/m³
 V_C = Velocity of vehicle, m/s

V_T	=	Velocity of air flow in tunnel, m/s	
C_d	=	Vehicle drag coefficient	= 0.645
A_c	=	Vehicle frontal area	= 4.0096 m ²
N	=	No. of vehicles in tunnel	
K_{in}	=	Inlet loss coefficient	= 0.5
K_{out}	=	Outlet loss coefficient	= 1.0
f	=	Tunnel friction factor	= 0.0155
L	=	Length of tunnel	= 48 m
D	=	Hydraulic diameter of tunnel = $4A_T/P$	= 8.470588 m, P is the Perimeter of tunnel
A_T	=	Cross-sectional area of tunnel	= 72 m ²
C_w	=	External wind coefficient	= 0.3
V_w	=	Velocity of wind	= 2.38 m/s (Weighted average of 1994 Junk Bay Station data)
θ	=	Angle of the wind velocity component parallel to the roadway	

For the worst scenario, only external wind at the exit portal is considered and the wind is parallel to the roadway.

$$\text{Force balance : } F_c - F_T - F_w = 0 \quad (1)$$

$$\text{Solving the equation, } a V_T^2 + b V_T + c = 0$$

where

$$a = C_d A_c N - (K_{in} + K_{out} + \frac{fL}{D}) A_T$$

$$b = -2 C_d A_c N V_w$$

$$c = C_d A_c N V_w^2 - C_w V_w^2 A_T$$

For normal traffic condition

$$\text{traffic flow } Q = 0.174167 \text{ veh/s}$$

$$\text{Vehicle speed } V_c = 50 \text{ km/h}$$

$$= 13.88889 \text{ m/s}$$

$$\text{Number of vehicles in tunnel } N = QL/V_c$$

$$= 0.60192$$

Solving for V_T by equation (1)

$$a = -112.77$$

$$b = -43.24$$

$$c = 177.93$$

$$\text{tunnel air flow velocity } V_T = 1.078962 \text{ m/sec} \quad \text{or} \quad -1.46242 \text{ m/sec}$$

(rejected)

$$\text{Inside tunnel concentration} = \text{emission rate} / (\text{tunnel air flow} \times \text{underpass cross-sectional area})$$

$$= 22.96477 \text{ ug/m}^3$$

For congested traffic condition

$$\text{Vehicle speed } V_c = 10 \text{ km/h}$$

$$= 2.777778 \text{ m/s}$$

$$\text{average length of vehicle} = (0.03+0.67)*4.6+0.06*6.5+0.11*5.2+0.05*16+0.08*12$$

$$= 5.942 \text{ m}$$

$$\text{distance between vehicle} = 1 \text{ m}$$

$$\text{head to head length} = 6.942 \text{ m}$$

$$\text{Number of vehicles per lane} = 6.914434$$

$$\text{Number of lanes} = 1$$

$$\text{Number of vehicles in tunnel } N = 6.914434$$

Solving for V_T by equation (1)

$$a = -96.44$$

$$b = -99.34$$

$$c = 15.63$$

$$\text{tunnel air flow velocity } V_T = 0.138647 \text{ m/sec} \quad \text{or} \quad -1.16875 \text{ m/sec}$$

(rejected)

$$\text{Inside tunnel concentration} = \text{emission rate} / (\text{tunnel air flow} \times \text{underpass cross-sectional area})$$

$$= 178.7135 \text{ ug/m}^3$$

Background Concentration

Four assessment points (ASR P5-P8) at the boundary of the Long Section of the underpass are chosen (see Figure A3). Using CALINE4 model, the NO2 concentrations at the 4 assessment points at different levels are calculated. Sample output file is shown in Appendix 4.7.

The highest concentration among the four assessment points is assumed to be the background NO2 concentration inside the Short Section of the underpass.

Without proposed noise barriers:

ASRs	NO2 Concentrations (ug/m3) at Various Levels below Lei Yue Mun Road		
	0m	4.5m	9m
P5	373	365	353
P6	380	416	397
P7	382	423	408
P8	452	514	516
The highest background concentration is			516 ug/m3

With proposed noise barriers:

ASRs	NO2 Concentrations (ug/m3) at Various Levels below Lei Yue Mun Road		
	0m	4.5m	9m
P5	373	365	353
P6	380	416	397
P7	382	423	408
P8	452	514	516
The highest background concentration is			516 ug/m3

Overall Maximum NO2 concentration inside the Underpass under Normal Condition

$$= 23 + 516 \quad \text{ug/m3}$$

$$= 539 \quad \text{ug/m3}$$

Overall Maximum NO2 concentration inside the Underpass under Worst Condition

$$= 179 + 516 \quad \text{ug/m3}$$

$$= 695 \quad \text{ug/m3}$$