

FORM 5
ENVIRONMENTAL IMPACT ASSESSMENT ORDINANCE
(CHAPTER 499)
SECTION 13(1)

Application for Variation of an Environmental Permit

PART A PREVIOUS APPLICATIONS

No previous application for variation of an environmental permit.
 The environmental permit was previously amended.
Application No. : VEP-452/2014

PART B DETAILS OF APPLICANT

B1. Name : (person or company)
MTR Corporation Limited
[Note : In accordance with section 13(1) of the Ordinance, the person holding an environmental permit or a person who assumes responsibility for the designated project may apply for variation of the environmental permit.]
B2. Business Registration No. : [REDACTED]
(if applicable)
B3. Correspondence Address : [REDACTED]
B4. Name of Contact Person : [REDACTED]
B5. Position of Contact Person : [REDACTED]
B6. Telephone No. : [REDACTED]
B7. Fax No. : [REDACTED]
B8. E-mail Address : (if any) [REDACTED]

PART C DETAILS OF CURRENT ENVIRONMENTAL PERMIT

C1. Name of the Current Environmental Permit Holder :
MTR Corporation Limited
C2. Application No. of the Current Environmental Permit : EP-313/2008/J
C3. The Current Environmental Permit was issued in : month / year
09 / 2014

Important Notes : Please submit the application together with
(a) 3 copies of this completed form; and
(b) appropriate fee as stipulated in the Environmental Impact Assessment (Fees) Regulation
to the Environmental Protection Department at the following address :
The EIA Ordinance Register Office,
27th floor, Southorn Centre, 130 Hennessy Road,
Wan Chai, Hong Kong.

Tick (✓) the appropriate box



PART D PROPOSED VARIATIONS TO THE CONDITIONS IN CURRENT ENVIRONMENTAL PERMIT

D1. Condition(s) in the Current Environmental Permit :	D2. Proposed Variation(s) :	D3. Reason for Variation(s) :	D4. Describe the environmental changes arising from the proposed variation(s) :	D5. Describe how the environment and the community might be affected by the proposed variation(s) :	D6. Describe how and to what extent the environmental performance requirements set out in the EIA report previously approved or project profile previously submitted for this project may be affected :	D7. Describe any additional measures proposed to eliminate, reduce or control any adverse environmental impact arising from the proposed variation(s) and to meet the requirements in the Technical Memorandum on Environmental Impact Assessment Process :
<p>Condition 4.1.2:</p> <p>In accordance with the approved EIA Report and other relevant documents on the Register, only Metro-Cammell (M-stock) trains, C-stock trains, and/or K-stock trains shall be deployed in the Project, subject to full and proper implementation of the measures, if any, recommended in the noise performance test report deposited under Condition 4.1.6 below. The maximum nighttime (23:00 hour to 07:00 hour) train frequency operating in the Project shall be limited to 10 trains per 30 minutes in each direction. The total length of the trains shall not be longer than 200m.</p>	<p>Condition 4.1.2:</p> <p>Unless otherwise approved by the Director subject to the submission of a detailed proposal, the operation details given below shall be adopted:</p> <p>In accordance with the approved EIA Report and other relevant documents on the Register, only Metro-Cammell (M-stock) trains, C-stock trains, K-stock trains, or Q-stock trains shall be deployed in the Project, subject to full and proper implementation of the measures, if any, recommended in the Noise Performance Test Report deposited under Condition 4.1.6 below and the detailed proposal submitted under Condition 4.1.2. The maximum nighttime (23:00 hour to 07:00 hour) train frequency operating in the Project shall be limited to 10 trains per 30 minutes in each direction. The total length of the trains shall not be longer than 200m.</p>	<p>As part of the long-term asset renewal strategy to sustain high quality railway service for passengers, MTRCL has procured new Q-stock trains to replace all the existing first-generation M-stock trains running on the urban lines in phases.</p> <p>In accordance with the FDL Measurement Report given in Annex A of the VEP application supporting document, the Force Density Levels (FDLs) of the Q-stock is lower than that of the M-stock trains adopted in the approved WIL EIA Report.</p>	<p>With the same set of trackform proposed in the approved WIL EIA Report, the predicted ground-borne noise levels at the identified existing Noise Sensitive Receivers, as presented in Table 4.10 of the approved WIL EIA Report, will be the same or reduced.</p> <p>Please refer to Table 3.1 of the VEP application supporting document.</p>	<p>There will not be any adverse impact on the environment or the community from the proposed variation, either directly or indirectly.</p>	<p>With proper mitigation measures in place, the environmental impact of WIL will not exceed/violate the environmental performance requirements set in the approved EIA Report.</p> <p>Please refer to Sections 2 and 3 of the VEP application supporting document.</p>	<p>The requirements in the EIAO-TM are complied with. No additional measure is required.</p>

PART E DECLARATION BY APPLICANT

E1. I hereby certify that the particulars given above are correct and true to the best of my knowledge and belief. I understand the environmental permit may be suspended, varied or cancelled if any information given above is false, misleading, wrong or incomplete.

Signature of Applicant

Full Name in Block Letters

Position



on behalf of _____
Company Name and Chop (as appropriate)

24/10/2018
Date

NOTES :

1. A person who constructs or operates a designated project in Part I of Schedule 2 of the Ordinance or decommissions a designated project listed in Part II of Schedule 2 of the Ordinance without an environmental permit or contrary to the permit conditions commits an offence under the Ordinance and is liable to a maximum fine of \$5,000,000 and to a maximum imprisonment for 2 years.
2. A person for whom a designated project is constructed, operated or decommissioned and who permits the carrying out of the designated project in contravention of the Ordinance commits an offence and is liable to a maximum fine of \$5,000,000 and to a maximum imprisonment for 2 years.

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MTR Corporation Limited

Review Report for the Use of Q- stock Trains in WIL

October 2018

Environmental Resources Management

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EIAO
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MTR Corporation Limited

Review Report for the Use of Q-stock Trains in WIL

October 2018

Reference 0432570

For and on behalf of ERM-Hong Kong, Limited	
Approved by:	Frank Wan
Signed:	<i>Frank Wan</i>
Position:	Partner
Date:	23 October 2018

This report has been prepared by ERM-Hong Kong, Limited with all reasonable skill, care and diligence within the terms of the Contract with the client, incorporating our General Terms and Conditions of Business and taking account of the resources devoted to it by agreement with the client.

We disclaim any responsibility to the client and others in respect of any matters outside the scope of the above.

This report is confidential to the client and we accept no responsibility of whatsoever nature to third parties to whom this report, or any part thereof, is made known. Any such party relies on the report at their own risk.

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BACKGROUND

Following the approval of the West Island Line (WIL) Environmental Impact Assessment (EIA) Report ^[1] on 23 December 2008, an Environmental Permit (EP) (EP-313/2008) was granted for the WIL on 12 January 2009. Further amendments to the EP were approved from 2009 to 2014, including a Variation of EP (VEP) in February 2014 to allow the use of C-stock trains and K-stock trains. The WIL (hereafter referred to as the Project) is now operating by the MTR Corporation Limited (MTRCL).

In accordance with Condition 4.1.2 of the current WIL EP (EP-313/2008/J), “only Metro-Cammell (M-stock) trains, C-stock trains, and/or K-stock trains shall be deployed in the Project”. As part of the long-term asset renewal strategy to sustain high quality railway service for passengers, MTRCL has procured new Q-stock trains to replace all the existing first-generation M-stock trains running on the urban lines in phases.

In accordance with Section 8.5.2.8 of the approved Kwun Tong Line Extension (KTE) Environmental Impact Assessment (EIA) Report ^[2], the Force Density Level (FDL) of M-stock is higher than that of K-stock trains considering that M-stock trains have a cast iron brake system which tends to cause more rail wear and more vibration than the disc brake system comparing with K-stock trains. According to the approved ERR in support of the VEP for the use of C-Stock trains and K-stock trains, the FDL of C-Stock trains was measured and shown to be lower than the FDL of M-Stock trains in the approved WIL EIA Report, and therefore, ground-borne noise impact by C-Stock trains was considered to be lower than that by M-Stock trains. Based on the above, the FDL of the Q-stock trains has been measured and the source term for the Q-stock trains has been compared with those assumed for the M-stock (i.e. the worst train) in the approved WIL EIA Report.

To support the application for this VEP, supplementary information has been provided in this *Report* (hereafter referred to as the Review) to demonstrate that the proposed variation will not cause adverse environmental impact and hence will not constitute a material change to the Project with respect to the requirements of the *Technical Memorandum on Environmental Impact Assessment Process (EIAO-TM)*.

[1] West Island Line Environmental Impact Assessment Report (Register No.: AEIAR-126/2008) (WIL EIA Report)

[2] Kwun Tong Line Extension Environmental Impact Assessment Report (Register No.: AEIAR-154/2010) (KTE EIA Report)

1.2 *PURPOSE OF THIS REPORT*

This *Report* presents the findings of a review of the potential environmental impacts that may arise from the proposed use of Q-stock trains in WIL.

1.3 *REPORT STRUCTURE*

The remainder of this *Report* is set out as follows:

- *Section 2* describes the proposed variations and the associated potential environmental issues;
- *Section 3* presents a review of the potential environmental impacts due to the proposed variation; compares the results with that presented in the approved WIL EIA Report; and review the requirements for further environmental mitigation measures;
- *Section 4* provides a review of the environmental monitoring and audit requirements; and
- *Section 5* provides a conclusion of the Review.

2.1 PROPOSED VARIATION

As explained in *Section 1*, MTRCL proposes to use Q-stock trains to replace all the existing first-generation M-stock trains in phases. Based on this, it is proposed to amend Condition 4.1.2 of the current WIL EP. Details of the proposed amendment are given below and in the VEP application form.

Condition 4.1.2:

Unless otherwise approved by the Director subject to the submission of a detailed proposal, the operation details given below shall be adopted:

In accordance with the approved EIA Report and other relevant documents on the Register, only Metro-Cammell (M-stock) trains, C-stock trains, K-stock trains, or Q-stock trains shall be deployed in the Project, subject to full and proper implementation of the measures, if any, recommended in the Noise Performance Test Report deposited under Condition 4.1.6 below and the detailed proposal submitted under Condition 4.1.2. The maximum nighttime (23:00 hour to 07:00 hour) train frequency operating in the Project shall be limited to 10 trains per 30 minutes in each direction. The total length of the trains shall not be longer than 200m.

2.2 POTENTIAL ENVIRONMENTAL IMPACTS

Table 2.1 identifies the potential sources of environmental impacts associated with the proposed variation.

Table 2.1 Potential Environmental Issues during Operation

Type of Potential Impacts	Potential Impacts Arising from the Proposed Changes
Air-borne noise	✘
Ground-borne noise	✓
Air quality	✘
Landscape	✘
Visual	✘
Ecology	✘
Fisheries	✘
Water quality	✘
Waste arisings	✘
Land contamination	✘
Hazard to life	✘
Cultural heritage	✘
✓ possible ✘ not expected	

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3.1**GROUND-BORNE NOISE IMPACT**

In the approved WIL EIA Report, M-stock trains were assumed in the ground-borne noise (GBN) impact assessment, which was conducted based on the FDL of the M-stock trains presented in Appendix 4.5 of the approved WIL EIA Report.

With the proposed variation, the FDL of the Q-stock trains has been measured and the source term for the Q-stock trains has been compared with those for the M-stock trains adopted in the approved WIL EIA Report.

The measurement results indicate that the FDL of the Q-stock trains is generally lower than that of the M-stock trains assumed in the approved WIL EIA Report. There is significant improvement in the FDL of the Q-stock trains at most of the frequencies, except 20Hz which has negligible contribution in calculating A-weighted ground-borne noise level. Details of the methodology and results of the FDL measurement for the Q-stock trains and comparison with the M-stock trains FDL assumed in the approved WIL EIA Report are given in *Annex A*.

With the reduction in the FDL, it is anticipated that GBN impact arising from the operation of the Q-stock trains will be lower than that from M-stock trains. Based on the above, the predicted GBN levels at the identified Ground-borne Noise Sensitive Receivers (GBNSRs), as presented in Table 4.10 of the approved WIL EIA Report, will be reduced.

A sample calculation of ground-borne noise impact at Hongway Garden (the worst affected NSR under worst case scenario) based on the FDL of the Q-stock trains is presented in *Annex B*. Assumptions, including train speed, train frequency, trackform attenuation and turnout and crossover factor, adopted in the sample calculation are the same as that in the approved EIA Report. The predicted GBN level at Hongway Garden, comparing with that predicted in the approved WIL EIA Report is presented in *Table 3.1*. The GBN level predicted in the approved WIL EIA Report is based on the assumption that all trains are M-stock. The GBN level predicted in this *Report* is based on the assumption that all trains are Q-stock. In actual operation, the fleet would be a mix of M-stock, C-stock, K-stock and Q-stock trains. The expected GBN level would be between the 2 predicted values presented in the approved WIL EIA Report and this *Report* (i.e. will not be greater than that predicted in the approved WIL EIA Report).

Table 3.1 *Predicted Ground-borne Noise Level and Comparing with the Approved WIL EIA Report*

GBNSR No.	Location	Criteria	GBN level predicted in the approved WIL EIA Report ^(a)	GBN level based on Q-stock Trains ^(b)
			dB(A) $L_{eq, 30min}$	
2	Hongway Garden	45	44	35

Notes:

- (a) Reference has been made from Table 4.10 of the approved WIL EIA Report, based on the assumption that all trains are M-stock.
- (b) GBN level predicted based on the assumption that all trains are Q-stock.

*REVIEW OF ENVIRONMENTAL MONITORING AND AUDIT
REQUIREMENTS*

No changes to the Environmental Monitoring and Audit Requirements as presented in the approved WIL EIA Report and the associated EM&A Manual will be required.

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CONCLUSIONS

An environmental review has been carried out to assess the potential environmental impacts associated with the proposed use of Q-stock trains to replace all the existing first-generation M-stock trains in WIL in phases. The assessment indicates that no adverse environmental impacts are anticipated from the proposed variation and the environmental performance requirements set out in the approved WIL EIA Report will not be exceeded.

It is proposed to amend Condition 4.1.2 of the current EP (EP No. EP-313/2008/J) of the WIL Project and details of the proposed amendment are given in the VEP application form.

The Project Proponent has reviewed the entire WIL Project as a whole, the proposed variation will not constitute a material change to the WIL Project and the Project fully complies with the EIAO-TM requirements.

Annex A

FDL Measurement Report

MTR Corporation Limited

FDL Measurement Report for the
Q-stock Trains for WIL and KTE

June 2018

Environmental Resources Management

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MEASUREMENT REPORT

MTR Corporation Limited

FDL Measurement Report for the
Q-stock Trains for WIL and KTE

June 2018

Reference 0432570

For and on behalf of ERM-Hong Kong, Limited	
Approved by:	Frank Wan
Signed:	
Position:	Partner
Date:	1 June 2018

This report has been prepared by ERM-Hong Kong, Limited with all reasonable skill, care and diligence within the terms of the Contract with the client, incorporating our General Terms and Conditions of Business and taking account of the resources devoted to it by agreement with the client.

We disclaim any responsibility to the client and others in respect of any matters outside the scope of the above.

This report is confidential to the client and we accept no responsibility of whatsoever nature to third parties to whom this report, or any part thereof, is made known. Any such party relies on the report at their own risk.

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As part of the long-term asset renewal strategy to sustain high quality railway service for passengers, MTR Corporation Limited (MTRCL) has procured new Q-stock trains to replace all the existing first-generation M-stock trains running on the urban lines.

The operation of West Island Line (WIL) and Kwun Tong Line Extension (KTE) are governed by the respective Environmental Permits (EPs) under the *Environmental Impact Assessment Ordinance* (EIAO). According to Condition 4.1.2 of the current WIL EP (EP-313/2008/J) and Condition 4.5 of the current KTE EP (EP-399/2010/D), only M-stock trains, K-stock trains and C-stock trains can be deployed. While MTRCL proposes to add Q-stock trains into the current train fleets, a variation of the current EPs (VEP) for WIL and KTE are thus required before the new trains can be deployed for service.

To support the application for VEP, supplementary information in terms of an Environmental Review Report (ERR) is prepared to demonstrate that the proposed change will not cause adverse environmental impact and hence will not constitute a material change to the WIL and KTE projects with respect to the requirements of the Technical Memorandum on Environmental Impact Assessment Process (EIAO-TM) and the respective approved EIA Reports.

As ground-borne noise would be one of the potential sources of environmental impacts associated with the proposed use of new Q-stock trains, it is necessary to measure the Force Density Level (FDL) of Q-stock trains and compare the source term for Q-stock trains with those assumed for M-stock trains. In accordance with Section 8.5.2.8 of the approved KTE EIA Report (Register No.: AEIAR-154/2010), the Force Density Level (FDL) of M-stock is higher than that of K-stock trains considering that M-stock trains have a cast iron brake system which tends to cause more rail wear and more vibration than the disc brake system comparing with K-stock trains. According to the approved ERR for the use of C-Stock trains, the FDL of C-Stock trains was measured and shown to be lower than the FDL of M-Stock trains in the approved WIL EIA Report, and therefore, ground-borne noise impact by C-Stock trains was considered to be lower than that by M-Stock trains. Based on the same approach, the FDL of the Q-stock trains will be measured and the source term for the Q-stock trains will be compared with those assumed for the M-stock (i.e. the worst train) in the approved EIA Reports.

ERM-Hong Kong, Limited (ERM) was commissioned by MTRCL as the Environmental Consultant for the environmental review in supporting the VEP application. ERM is supported by Wilson Acoustics Limited (WAL) who acts as the ground-borne noise specialist for the study.

1.2

PURPOSE OF THIS REPORT

WAL was commissioned to conduct the FDL measurement of Q-stock trains and compare with that of the M-stock trains assumed in the approved EIA Reports for the purpose of applications for VEP for WIL and KTE.

This *FDL Measurement Report* presents the methodology and results of the FDL measurement for Q-stock trains.

2.1

FDL DETERMINATION PROCEDURE

A schematic diagram showing the FDL measurement arrangement is shown in *Figure 2.1*. The measurement comprises two parts, the Line Source Response (LSR) measurement by hammer impact test, and the measurement of vibration level during train passage of a Q-stock test train.

FDL is determined by subtracting train induced vibration by LSR in logarithmic scale according to the equation below (*reference: "Transit Noise and Vibration Impact Assessment, FTA-VA-90-1003-06, published by US Federal Transit Administration" (FTA Manual)*):

$$FDL(f) = L_v(f, x, y, z) - LSR(f, x, y, z)$$

where

$L_v(f, x, y, z)$ = Train passby vibration level at ground surface outside building structure in dB re $10^{-9}m/s$ (in SI unit) or dB re $10^{-6}in/s$ (in Imperial unit), as a function of vibration frequency f and the sensor coordinate x, y, z .

$FDL(f)$ = Force Density Level in dB re $N/m^{0.5}$ (in SI unit) or dB re $1lb/ft^{0.5}$ (in Imperial unit), as a function of frequency f . FDL depends on the geology and train operating conditions.

$LSR(f, x, y, z)$ = Line Source Response from tunnel face to ground in dB re $(10^{-9}m/s)/(N/m^{0.5})$ (in SI unit) or dB re $(10^{-6}in/s)/(lb/ft^{0.5})$ (in Imperial unit), as a function of vibration frequency f and the sensor coordinate x, y, z .

Accelerometers were deployed at the rail and on ground surface at five various setbacks from the alignment which were 4.2m, 13.6m, 20.3m, 28.9m and 38.5m, respectively. Train passby vibration data L_v in 1/3-octave bands were captured for further analysis.

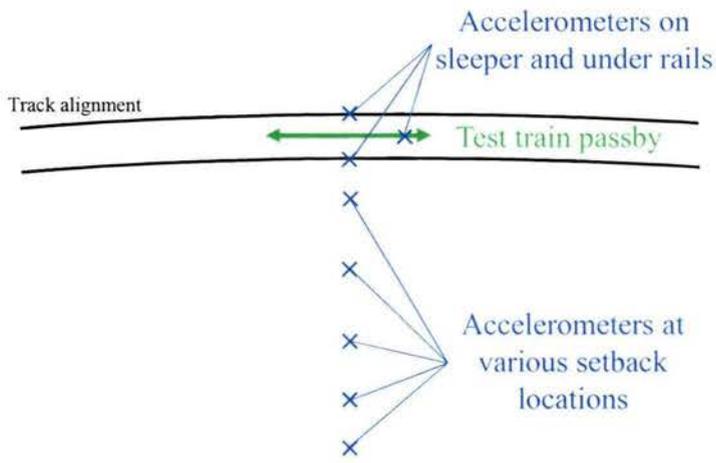
Hammer impact test was conducted to determine the soil mobility of the test site. The impact conducted consecutively gives the Point Source Response (PSR) at individual setback locations. LSR is calculated from numerical integration of the PSR along the alignment for each individual 1/3-octave band.

The FDL was then deduced by L_v and LSR.

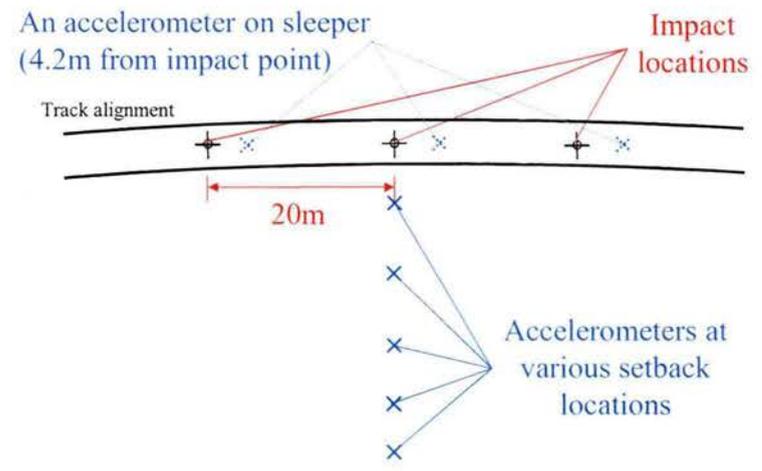
2.2

MEASUREMENT LOCATION

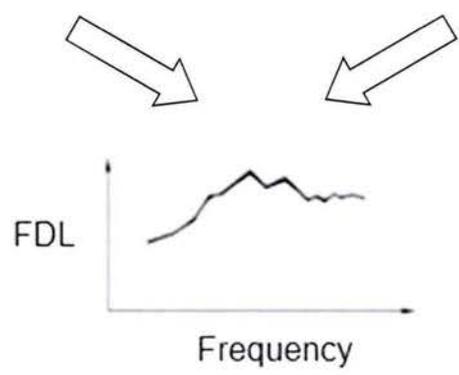
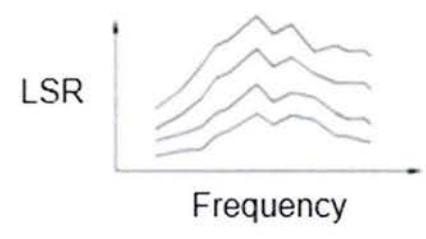
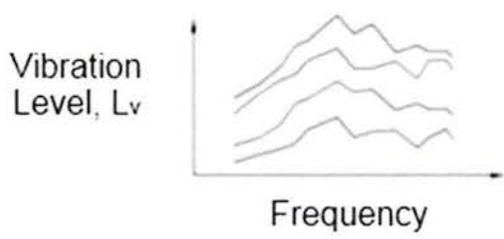
The Q-stock FDL measurement was performed at a ballast track section at Siu Ho Wan Depot test track. The FDL measurement locations are shown in *Figure 2.2*.



Vibration Measurement for Test Train Passby



LSR Measurement by Hammer Impact Test



$$FDL = L_v - LSR$$

Figure 2.1

FDL Analysis Procedure

Date 4 May 2018

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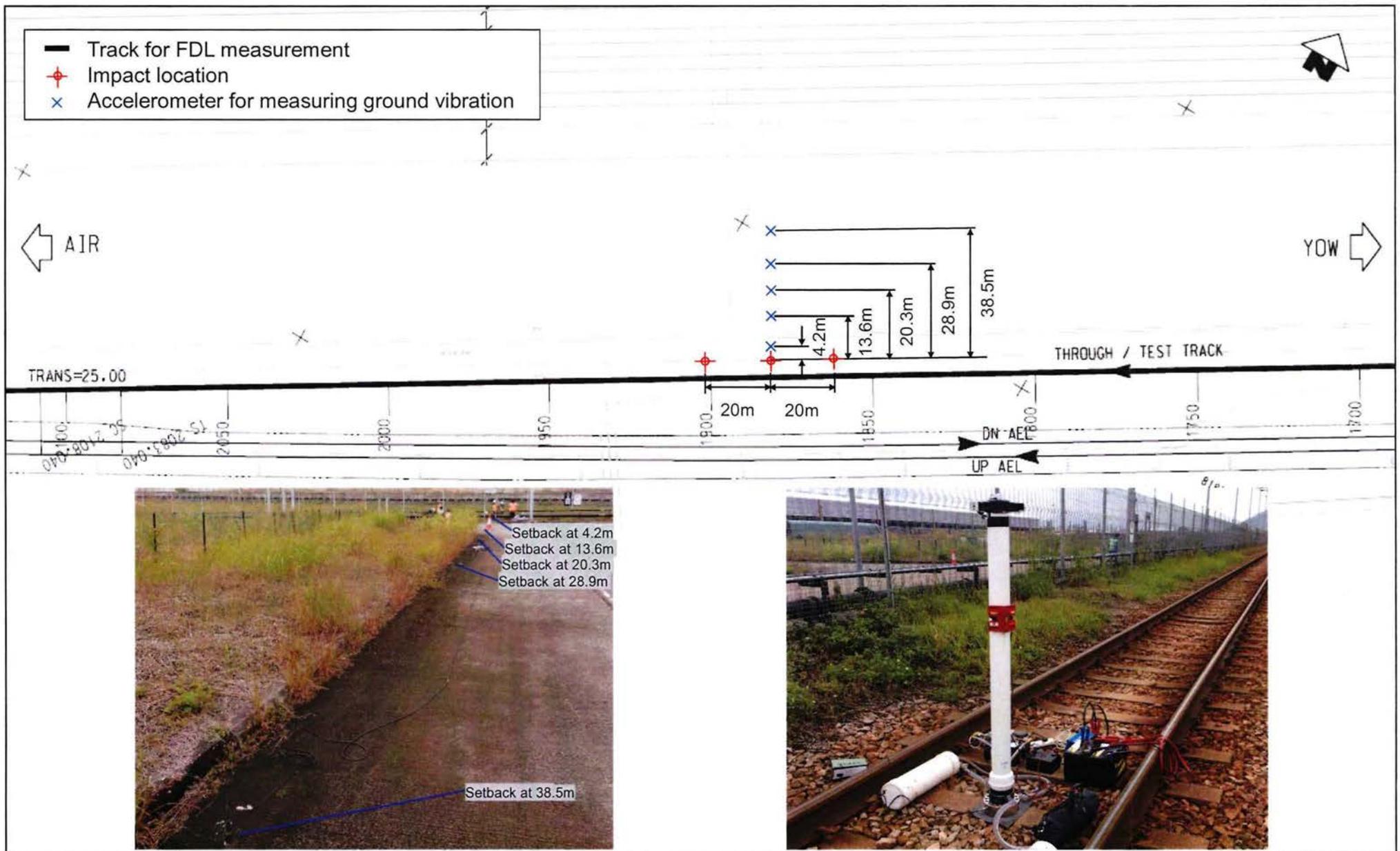


Figure 2.2

Location of Track for FDL Measurement

Date 4 May 2018

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2.3 MEASUREMENT SCHEDULE

The FDL measurement and the relevant activities were conducted on 14 March 2018, with the measurement schedule listed in *Table 2.1*.

Table 2.1 *Measurement Schedule*

Time	Measurement Activities
08:00 – 09:00	Entry to test track Accelerometers set up at track and setback locations
09:00 – 12:00	Vibration measurement for Q-stock test train (constant speeds at 60kph, 40kph and 30kph, respectively)
15:00 – 16:00	Entry to test track Set up of Impact Hammer
16:00 – 17:00	Hammer impact test at 3 locations, 5-10 impacts for each location
17:00 – 18:00	Rail corrugation measurement Removal of all measurement equipment from track and setback locations

2.4 WHEEL AND TRACK CONDITIONS

A Q-stock test train was deployed for FDL measurement. The train has no audible wheel-flats.

The test section was a continuously rail on ballast and sleepers.

The vibration level induced by train passage is related to rail roughness. Thus measuring rail roughness at the time of FDL measurement provides a good reference and record for comparison with future measurements.

Rail corrugation measurement was conducted in accordance with *BS EN 15610:2009 - Railway applications. Noise emission. Rail roughness measurement related to rolling noise generation* over a distance of 200m of each rail. Detailed measurement results are presented in *Appendix A*.

The acoustic rail roughness was in general higher than the limit of reference track condition recommended by *ISO 3095:2013 Acoustics – Railway Applications – Measurement of Noise Emitted by Railbound Vehicle* and *TSI 2011/229/EU Technical Specifications for Interoperability (TSI)*, which sets the roughness criteria for noise commissioning test. This indicated the measured FDL was not captured under perfect rail condition, which is conservative to the assessment of ground-borne noise impact arising from Q-stock trains.

Photos of the rail running surface are shown in *Appendix A*.

2.5 MEASUREMENT EQUIPMENT

Measurement instruments and vibration measurement locations are listed in *Table 2.2*. Photos of the measurement equipment are shown in *Figures 2.3* to *2.6*.



Figure 2.3

Brüel & Kjær Pulse Analyser 3050 with Laptop Computer

Date 4 May 2018

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CTC AC216-1A



PCB 393A03

Figure 2.4

Accelerometers

Date 4 May 2018

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Figure 2.5

WAL-001 Impact Hammer

Date 4 May 2018

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Figure 2.6

Corrugation Analysis Trolley (CAT)

Date 4 May 2018

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Similar to the approved WIL EIA Report, low sensitivity accelerometers were placed at the track and higher sensitivity accelerometers were placed on ground at setbacks. Sensor locations are listed in *Table 2.3*.

Table 2.2 *Measurement Instruments*

Instrument	Model No.	Qty.	Figure No.
6-Channel Spectrum Analyser	Brüel & Kjær Pulse 3050	2	2.3
Piezoelectric Accelerometer	CTC AC216-1A	3	2.4
Piezoelectric Accelerometer	PCB 393A03	5	2.4
Vibration Calibrator	IMI 699A02	1	
Impact Hammer	WAL-001	1	2.5
Corrugation Analysis Trolley (CAT)	Rail Measurement CAT 3	1	2.6

Table 2.3 *Deployment of Vibration Sensors*

Location (Figure 2.2)	Accelerometer	Sensitivity
Under left rail	CTC AC216-1A #1	100mV/g
Under right rail	CTC AC216-1A #2	100mV/g
On sleeper (4.2m from impact point)	CTC AC216-1A #3	100mV/g
Setback at 4.2m (from track centreline)	PCB 393A03 #1	1V/g
Setback at 13.6m (from track centreline)	PCB 393A03 #2	1V/g
Setback at 20.3m (from track centreline)	PCB 393A03 #3	1V/g
Setback at 28.9m (from track centreline)	PCB 393A03 #4	1V/g
Setback at 38.5m (from track centreline)	PCB 393A03 #5	1V/g

2.6 MEASUREMENT PROCEDURE

For LSR measurement, hammer impact was conducted at 3 different locations along the alignment. For each location, 5-10 hammer impacts were conducted for averaging. LSR is determined by numerical integration of PSR along the alignment.

For train passby vibration measurement, the train run at constant speeds of 30kph, 40kph and 60kph. For each train speed, at least 3 passbys were measured.

3 MEASUREMENT RESULTS AND DISCUSSION

3.1 TRAIN PASSBY VIBRATION MEASUREMENT AND HAMMER IMPACT TEST RESULTS

Train passby vibration level and point source response as determined from hammer impact test are presented in *Appendix B*. The soil at the subject site has peak transfer mobility around 20-125Hz, while train vibration peaks around 20-80Hz.

The A-weighted train passby vibration level is plotted against log train speed. It shows that A-weighted vibration level follows approximately the relationship $\Delta L_v = 20 \log(\text{speed})$.

As A-weighted vibration level is directly correlated to the ground-borne noise level, double train speed results in approximately 6dB(A) increase in ground-borne noise level. The measurement results for Q-stock trains are similar to that for M-stock trains as presented in the approved EIA Reports, and also in line with the FTA manual.

3.2 FDL MEASUREMENT RESULT

The FDL for Q-stock trains is determined from the LSR and train passby vibration level at 60kph, and shown in *Figure 3.1*. Train speed 60kph is selected since the approved WIL EIA report only presents FDL at 60kph available for comparison. Since the correlations between vibration level and train speed are similar, it is anticipated that if FDL of Q-stock is lower than that of M-stock at 60kph, the FDL would also be lower at other train speeds.

Similar to the approved EIA Report, two standard deviations are added on top of the measured average FDL value, in order to account for uncertainties and variations in the measurement. The adjusted FDL value is also presented in *Figure 3.1*.

3.3 COMPARISON WITH EIA ADOPTED FDL

The FDL of Q-stock trains is compared with that of M-stock trains adopted in the approved EIA Reports, as shown in *Figure 3.2*. Both FDL values include two standard deviations to account for measurement uncertainties.

The FDL of Q-stock trains is found to be in general lower than that of the M-stock trains adopted in the approved EIA Reports except at 20 Hz. Considering the frequency at 20Hz has negligible contribution in calculating A-weighted ground-borne noise level and there are significant improvement of Q-stock FDL at other frequencies, it is anticipated that ground-borne noise impact arising from Q-stock trains will be lower than that from M-stock trains.

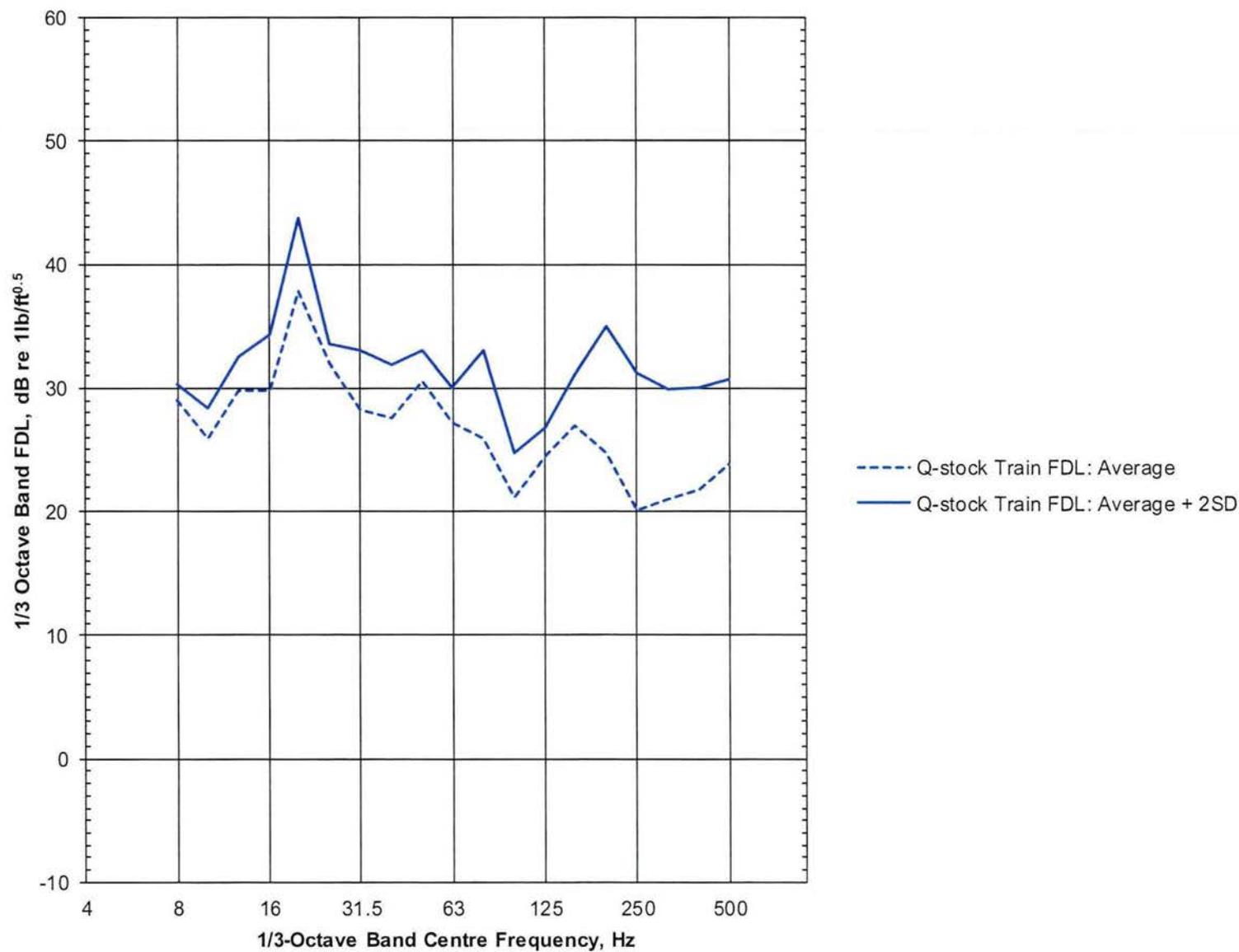


Figure 3.1

Siu Ho Wan Test Track Force Density Level

Date 4 May 2018

Environmental
Resources
Management



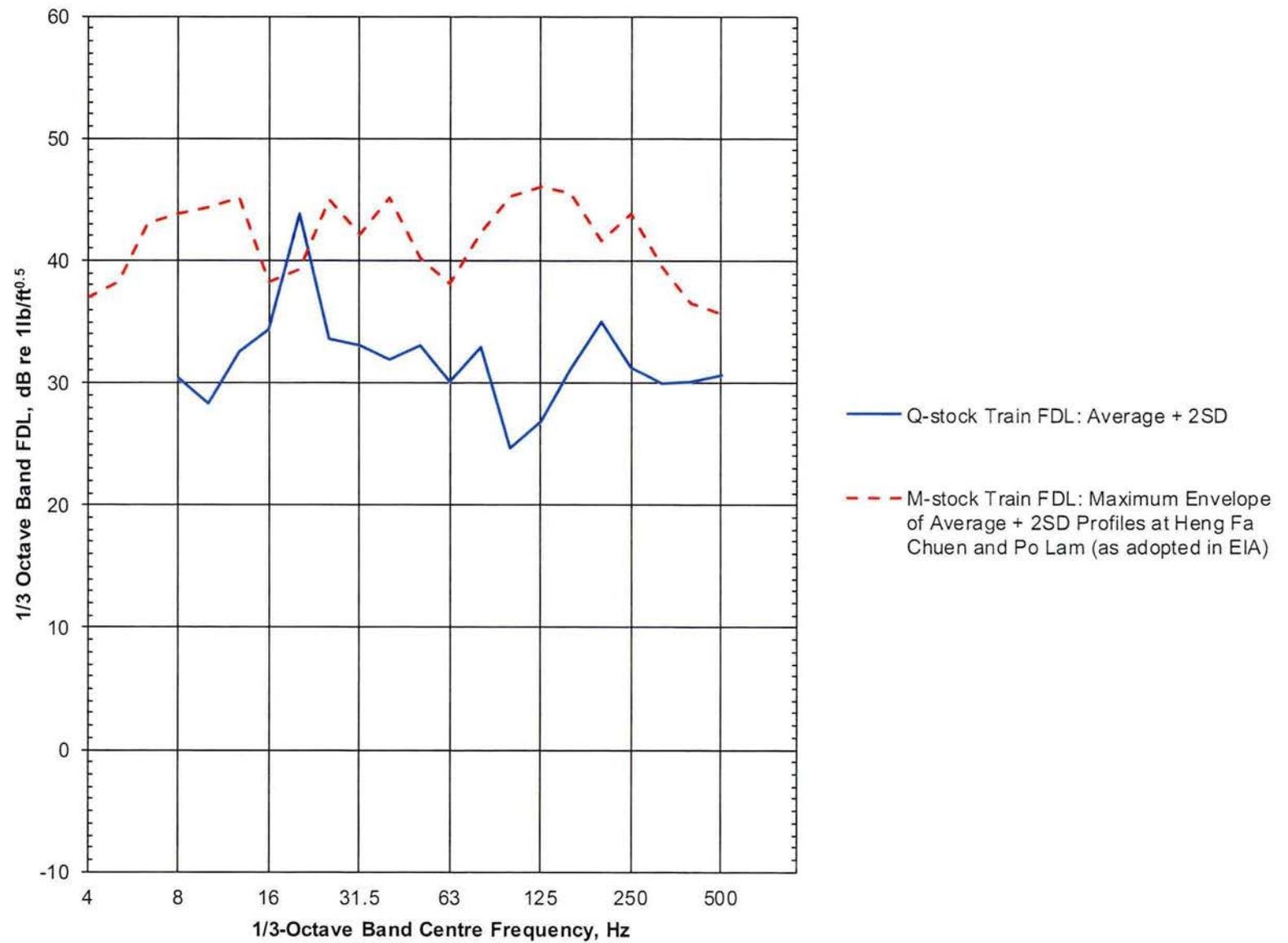


Figure 3.2

Force Density Levels of Q-stock and M-stock Trains

Date 4 May 2018

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Resources
Management



CONCLUSIONS

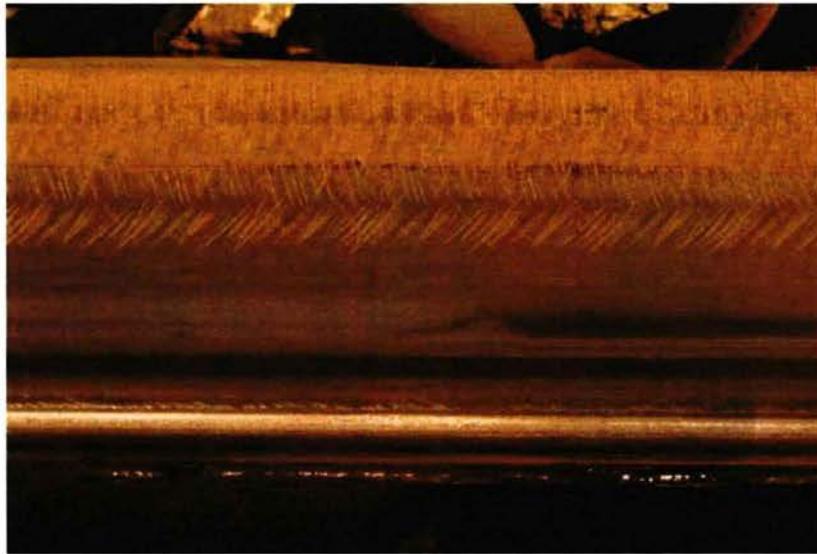
Q-stock FDL Measurement has been conducted at the test track of Siu Ho Wan Depot.

Results indicate that the A-weighted Q-stock passby vibration level increases with train speed approximately according to $20 \log(\text{speed})$. This is similar to that for the M-stock trains as presented in the approved EIA Reports.

The measured Q-stock FDL is found to be in general lower than the M-stock FDL adopted in the approved EIA Reports. Ground-borne noise impact arising from Q-stock trains is anticipated to be lower than that from M-stock trains.

Appendix A

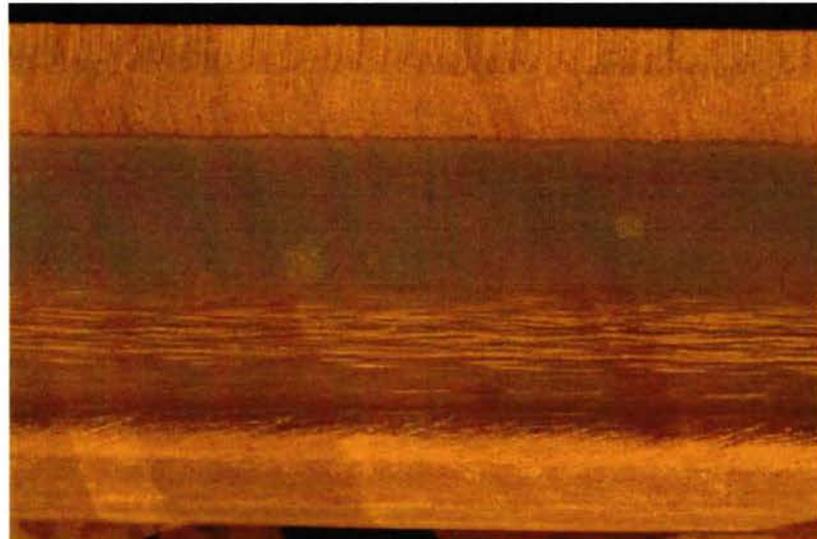
Rail Roughness Measurement Results



Running Surface of Far Rail
EIA



Running Surface of Far Rail
WAL



Running Surface of Near Rail



Running Surface of Near Rail

Figure A.1

Rail Surfaces during EIA measurement at Heng Fa Chuen and WAL measurement at Siu Ho Wan Depot

Date 4 May 2018

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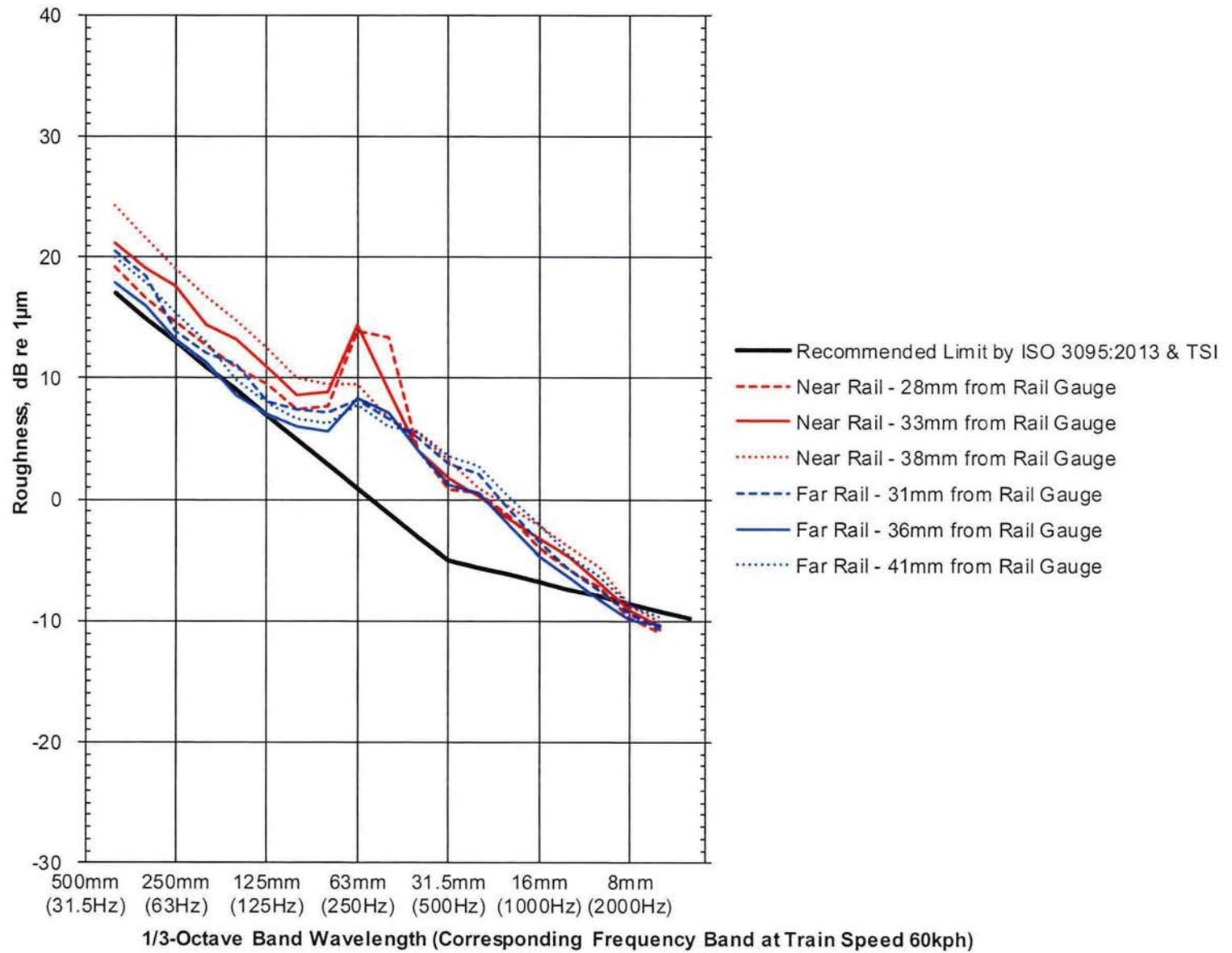


Figure A.2

Rail Roughness Spectra at Siu Ho Wan Test Track

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Appendix B

Train Passby Vibration and
Hammer Impact Test
Results

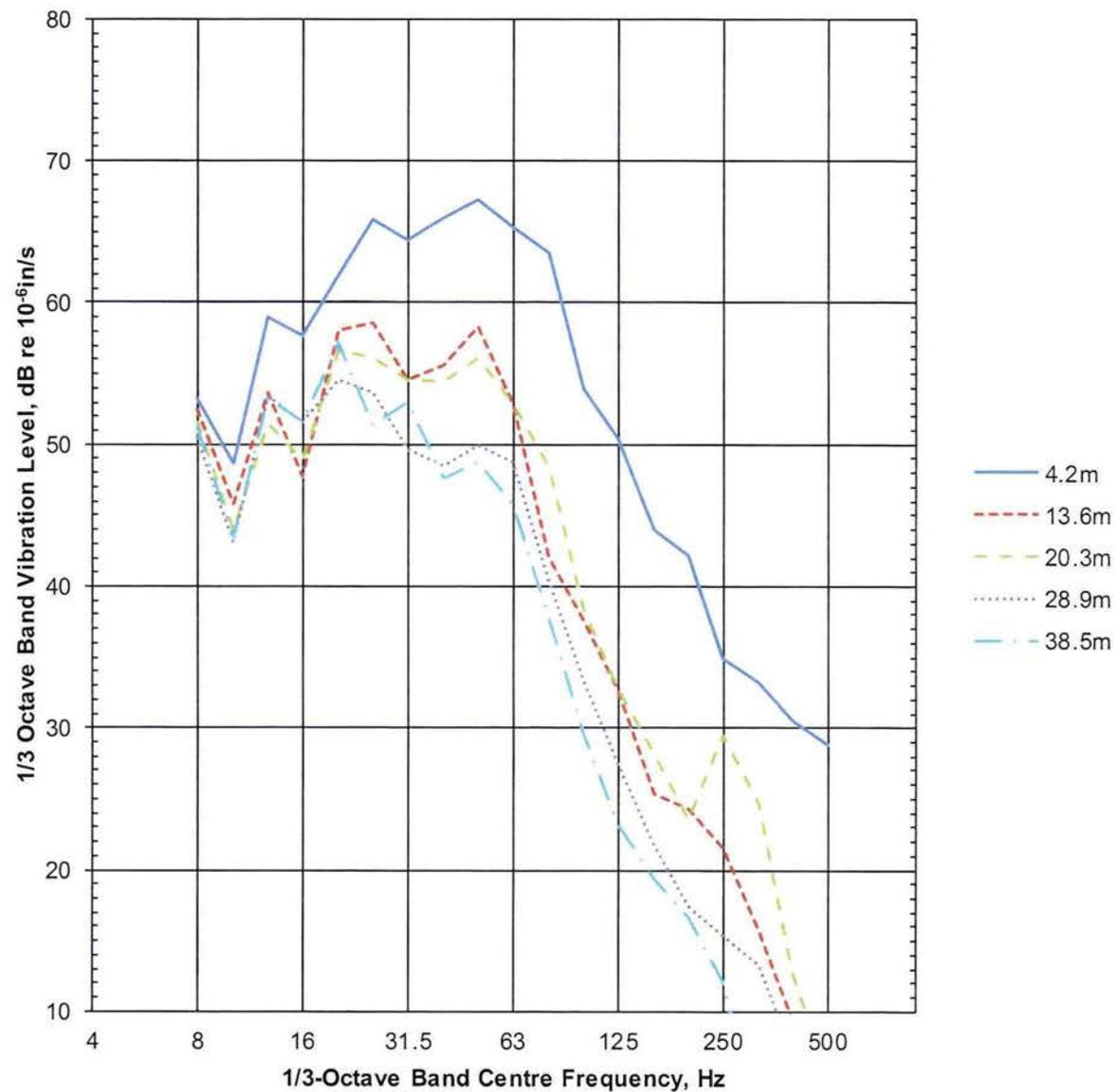


Figure B.1

Siu Ho Wan Test Track Q-stock Train Passby Vibration Levels at Different Setbacks

Date 4 May 2018

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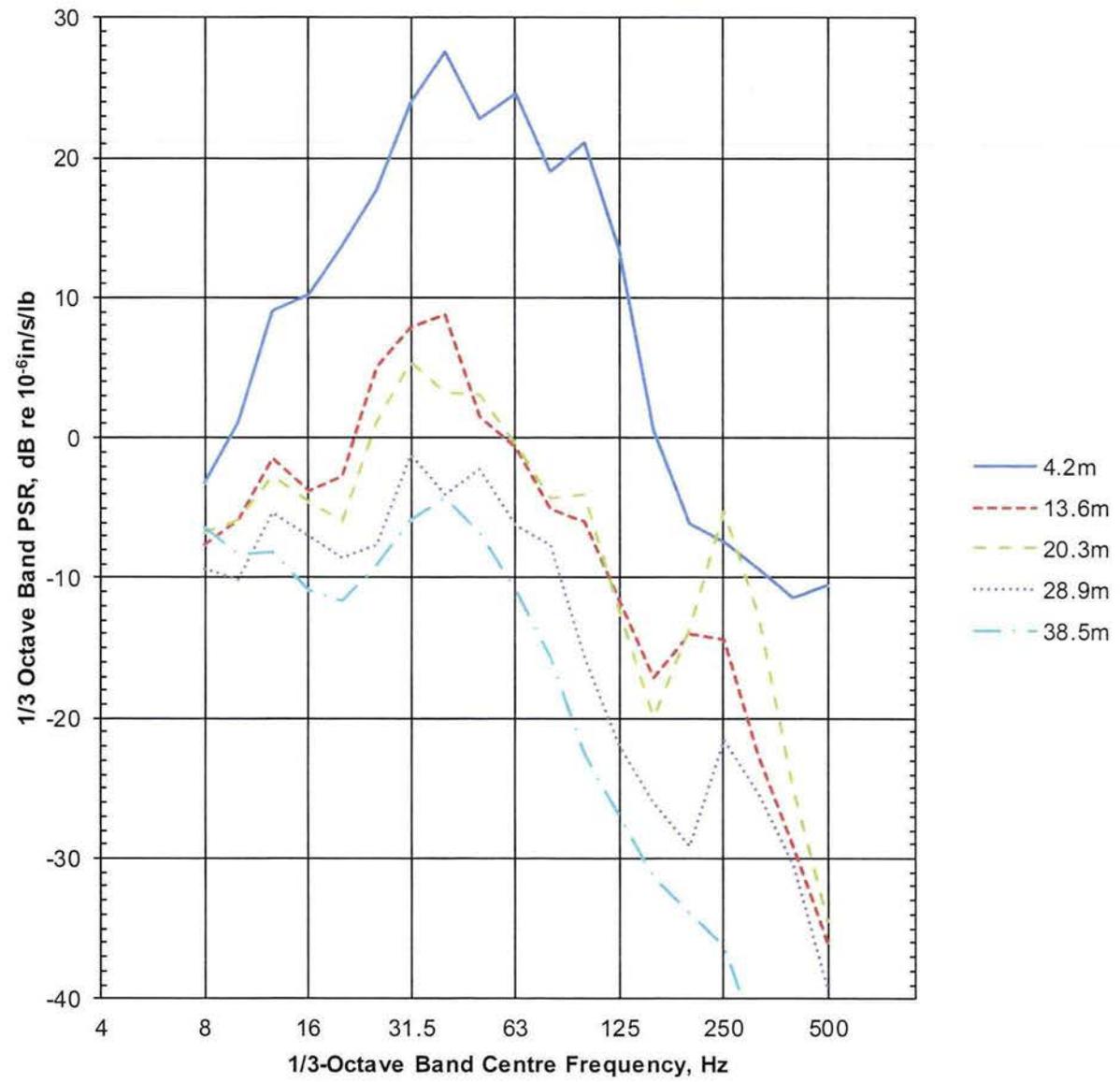


Figure B.2

Siu Ho Wan Test Track Point Source Responses at Different Setbacks

Date 4 May 2018

Environmental
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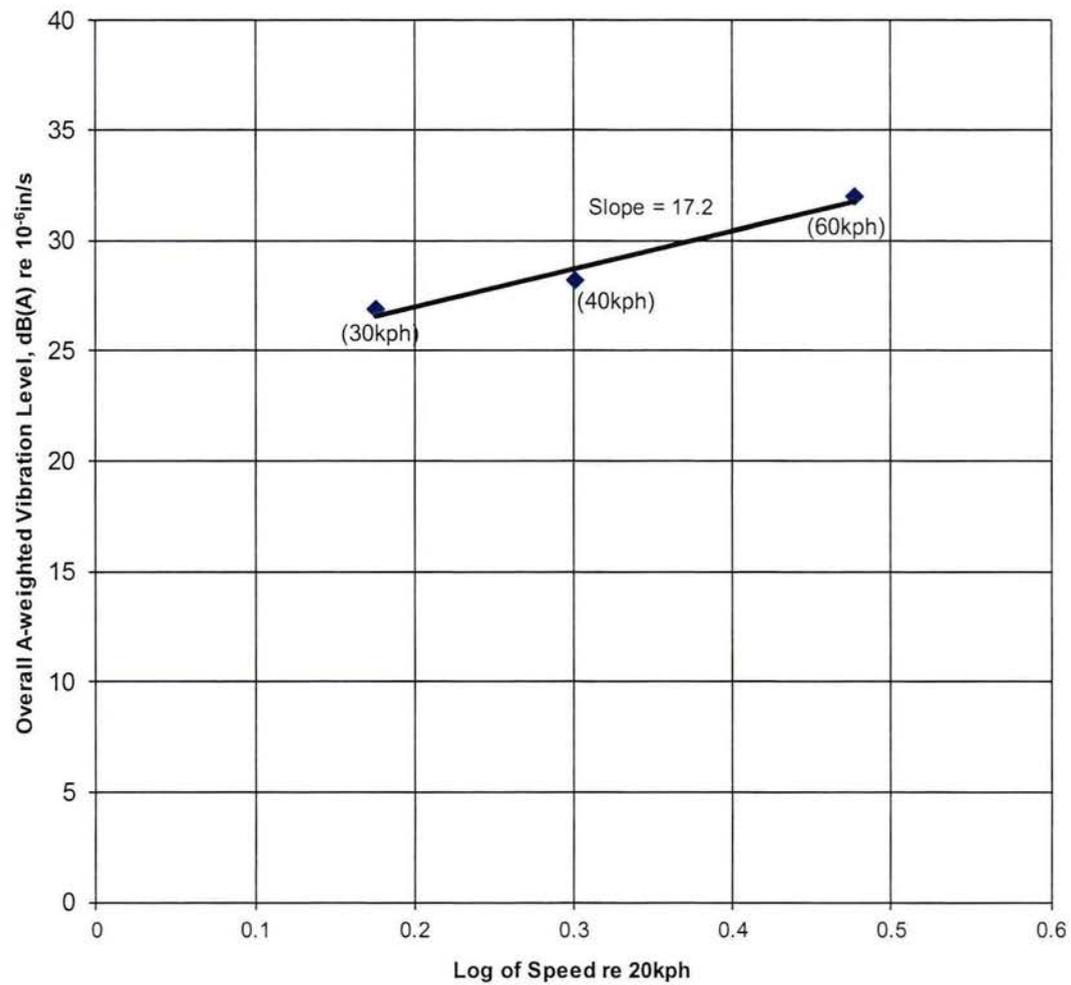


Figure B.3

Speed Correction for Overall A-Weighted Vibration Level

Date 4 May 2018

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Appendix C

Equipment Calibration Certificates

Wilson Acoustics Limited
Unit 601, Block A, Shatin Industrial Centre
Hong Kong



MANUFACTURER'S CERTIFICATE OF CONFORMANCE

We certify that Brüel & Kjær -3050-A-060- Serial No. 3050-100888 has been tested and passed all production tests, confirming compliance with the manufacturer's published specification at the date of the test.

The final test has been performed using calibrated equipment, traceable to national or international standards or by ratio measurements.

Brüel & Kjær is certified under ISO 9001:2008 assuring that all test data is retained on file and is available for inspection upon request.

Narum 16 dec. 2016


Torben Bjørn
Vice President, Operations

Please note that this document is not a calibration certificate.
For information on our calibration services please go to www.bk.com/cal

Reference number	Service request	Date
	CAS-120968-Z114RVV	29 Mar 2016

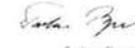
We hereby declare that

-3050-A-060- 6-ch Input Module LAN-XI 51.2kHz (Mic, CCLD, V) Serial Number: 3050-105894

has been tested and passed all test

The instrument has been tested according to published specifications at the date of the test
All tests have been performed using calibrated equipment, traceable to National or International Standards or by ratio measurements.

Certificate issued
29-Mar-2016


Torben Bjørn
Vice President - Operations
For and behalf of Brüel & Kjær HQ

Recommended date for next check: Mar-2017

Brüel & Kjær is certified under ISO 9001:2008, assuring that all calibration data is retained on file and is available for inspection upon request.

Note:
Although this certificate states that your equipment is compliant with specifications of its type, it does not show or guarantee accuracy.

Brüel & Kjær Sound & Vibration Measurement A/S
Sønderhojvej 317, 4104, 8050, Naerum, Denmark
Tel: +45 45 95 22 10 or +45 45 95 30 74, 21
E-mail: info@bksv.com
Website: www.bk.com

CVR nr. 22 90 94 14 • KAT nr. 04 11 00 00
Danish Bank Account no. 1100 3010 041260 SWIFT: DABN2222
IBAN: DK48 16 16 00 0000 0000 0000 0000
LSD: DK 75 3070 443 100 0004

Figure C.1

Calibration Certificates – Vibration Analyzer

Date 4 May 2018

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Resources
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校准报告
CALIBRATION REPORT

校准报告
CALIBRATION REPORT

报告编号: 130604733
Report No:

第 2 页, 共 5 页
Page 2 of 5 Pages



报告编号: 130604733

第 1 页, 共 5 页
Page 1 of 5 Pages

客户名称: 威信声学顾问有限公司
Name of Customer: Weixin Acoustic Consultant Co., Ltd.
客户地址: 香港新界沙田工业中心A座601
Address of Customer: 601, Industrial Centre A, Sha Tin, New Territories, Hong Kong
计量器具名称: 振动校准器
Name of Instrument: Vibration Calibrator
器具用途: _____
Use of Instrument: _____
型号/规格: 688A02
Type/Specification: 688A02
出厂编号: 389
Serial No: 389
资产编号: _____
Asset No: _____
制造单位: 1M1
Manufacturer: 1M1
校准依据: JJG 1062-2010 便携式振动校准器
Calibrate in Accordance with: JJG 1062-2010 Portable Vibration Calibrator



(校准专用章)
Stamp



校准日期: 2017 年 10 月 27 日
Calibration Date: Year Month Day
建议复校日期: 2018 年 10 月 26 日
Suggested Recal Date: Year Month Day

批准人: 张国庆(副所长)
Authorized by: Zhang Guoqing
签名: 张国庆
Signature: Zhang Guoqing
校验员: 李杰
Checked by: Li Jie
校准员: 李杰
Calibrated by: Li Jie

校准机构和备案号: 2012 粤量校 F002 号
地址: 深圳市南山区龙珠大道中理计量质检大楼
电话: (深圳) 215 2641546-1696 215 2641547
传真: 0086-755-2641543 0086-755-2641541
邮编: 518055 网站: www.smo.com.cn
电子邮箱: s1@smo.com.cn

Register No.: [2012]粤量校F002号
Add: Metrology and Quality Inspection Building Central Section of Longzhu Road,
Nanshan District Shenzhen
Tel: 0086-755-2641546 0086-755-2641540
Fax: 0086-755-2641543 0086-755-2641541
Post Code: 518055 Http://www.smo.com.cn
E-mail: s1@smo.com.cn

校准用主要计量标准装置信息
Main Standard Devices Used

名称 Equipment Name	测量范围 Measuring Range	不确定度/准确度等级/ 最大允许误差 Uncertainty/Accuracy Class/ Maximum Permissible Error	计量标准考核证书号 Certificate No.	有效期至 Due Date

校准用主要标准器信息
Main Standards of Measurement Used

名称 Equipment Name	测量范围 Measuring Range	不确定度/准确度等级/ 最大允许误差 Uncertainty/Accuracy Class/ Maximum Permissible Error	设备编号 Equipment No.	证书号 Certificate No.	有效期至 Due Date
振动校准器 Vibration Calibrator	0.2 Hz - 1000 Hz (±1%)	(1) ± 0.5%, (2) ± 1%	SBD421-02	LS-02017-0678	2018-09-14

附加说明
Appended Directions

委托日期: 2017 年 10 月 23 日
Application Date: 2017-10-23
校准地点: 本院声学振动实验室
Calibration Location: Acoustic Vibration Laboratory
环境条件: 温度 20℃ 相对湿度 50%
Calibration Environment: Temperature 20°C, Relative Humidity 50%
符合性及限制使用说明: 无校准项目(或项目)合格
Statement of Compliance and Limitation: No calibration items (or items) are qualified.

Figure C.2

Calibration Certificates – Vibration Calibrator (Pages 1 and 2 of 5)

Date 4 May 2018

校准报告
CALIBRATION REPORT

报告编号: 170901722
Report No:

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Page 4 of 5 Pages

校准结果
Results of Calibration

1. 外观检查: 正常

Appearance Check: Pass

2. 振动幅值:

Amplitude

2.1 加速度: 见表1

Acceleration: See Table 1

表1 Table 1

加速度标称值	加速度实测值	误差	最大允许误差
Nominal SPL	Measured SPL	Error	M.P.E.
(m/s ²)	(m/s ²)	(%)	(%)
9.8	9.75	+0.5	±3.0

2.2 等效位移: 见表2

Equivalent Displacement: See Table 2

表2 Table 2

速度标称值	速度实测值	误差	最大允许误差
Nominal SPL	Measured SPL	Error	M.P.E.
(mm/s)	(mm/s)	(%)	(%)

校准报告
CALIBRATION REPORT

报告编号: 170901722
Report No:

第 4 页, 共 5 页
Page 4 of 5 Pages

校准结果
Results of Calibration

9.8	9.75	+0.5	±3.0
-----	------	------	------

2.3 等效位移: 见表3

Equivalent Displacement: See Table 3

表3 Table 3

位移标称值	位移实测值	误差	最大允许误差
Nominal SPL	Measured SPL	Error	M.P.E.
(mm)	(mm)	(%)	(%)
9.8	9.75	+0.5	±3.0

3. 频率: 见表4

Frequency: see Table 4

表4 Table 4

频率标称值	频率实测值	误差	最大允许误差
Nominal Freq.	Measured Freq.	Error	M.P.E.
(Hz)	(Hz)	(%)	(%)
159.2	159.2	0.0	±1.0

4. 加速度谱密度: 见表5

Figure C.3

Calibration Certificates – Vibration Calibrator (Pages 3 and 4 of 5)

Date 4 May 2018



校准报告
CALIBRATION REPORT

报告编号: 71601233
Report No.

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Page 5 of 5 Pages

校准结果
Results of Calibration

WC Distortion See Table 5

表 5 Table 5

标称频率 Nominal Freq.	标称幅值 Nominal Amplitude	失真度 Distortion	允许范围 Limit
(Hz)	(m/s ²)	(%)	(%)
150.2	9.8	0.02	≤5.0

附注(Notes):

- 等效速度和等效位移由参考频率加速度换算得出。
- 加速度测量结果相对扩展不确定度: $k_{95} = 1.4\%$, $k = 2$

(依据 JJF1059.1-2012 测量不确定度评定及表示)

Related Expanded Uncertainty of Acceleration: $k_{95} = 1.4\%$, $k = 2$

(By JJF1059.1-2012 Evaluation and Expression of Uncertainty in Measurement)

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Figure C.4

Calibration Certificates – Vibration Calibrator (Page 5 of 5)

Date 4 May 2018

Annex B

Sample Ground-borne Noise Calculation

Project: WIL Operational Groundborne Noise Assessment
 NSR No.: 2 (Mitigated)
 NSR Name: Hongway Garden
 NSR Use: Residential
 No. of Basement Floors: 1
 NSR Floor: 2

	Slant Dist. m	Train Speed. kph	Passby in thr
Eastbound	23	80	20
Westbound	23	80	20

Descriptions	Unit	1/3 Octave Band Center Frequency																	
		8	10	12.5	16	20	25	31.5	40	50	63	80	100	125	160	200	250	315	400

Eastbound Vibration Calculation

FDL	dB re 1lb/ft ^{0.5}	32.8	30.8	35.0	36.9	46.3	36.1	35.5	34.3	35.6	32.5	35.5	27.2	29.3	33.6	37.5	33.7	32.4	32.6	33.1
LSR	dB re 1(μin/s)/(lb/ft ^{0.5})	7.8	6.0	-2.0	-3.3	-2.8	3.3	5.2	11.0	13.4	13.1	11.7	5.2	6.7	6.3	3.3	-0.5	2.2	1.0	-2.7
TOC	dB	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0
TIL	dB	1.0	0.0	0.0	-1.0	-4.0	-5.0	-3.0	-3.0	0.0	-9.0	-13.0	-10.0	-12.0	-12.0	-13.0	-12.0	-10.0	-5.0	-5.0
TCF	dB	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
Eastbound Vibration Level	dB re 1μin/s	46.6	41.8	38.0	37.6	44.5	39.4	42.7	47.3	54.0	41.6	39.2	27.4	29.0	32.9	32.8	26.2	29.6	33.6	30.4

Westbound Vibration Calculation

FDL	dB re 1lb/ft ^{0.5}	32.8	30.8	35.0	36.9	46.3	36.1	35.5	34.3	35.6	32.5	35.5	27.2	29.3	33.6	37.5	33.7	32.4	32.6	33.1
LSR	dB re 1(μin/s)/(lb/ft ^{0.5})	7.8	6.0	-2.0	-3.3	-2.8	3.3	5.2	11.0	13.4	13.1	11.7	5.2	6.7	6.3	3.3	-0.5	2.2	1.0	-2.7
TOC	dB	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0
TIL	dB	1.0	0.0	0.0	-1.0	-4.0	-5.0	-3.0	-3.0	0.0	-9.0	-13.0	-10.0	-12.0	-12.0	-13.0	-12.0	-10.0	-5.0	-5.0
TCF	dB	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
Westbound Vibration Level	dB re 1μin/s	46.6	41.8	38.0	37.6	44.5	39.4	42.7	47.3	54.0	41.6	39.2	27.4	29.0	32.9	32.8	26.2	29.6	33.6	30.4

Total of Eastbound and Westbound Groundborne Noise Calculation

Total Vibration Level Outside Building	dB re 1μin/s	49.6	44.8	41.0	40.6	47.5	42.4	45.7	50.4	57.0	44.7	42.2	30.4	32.0	35.9	35.8	29.2	32.6	36.6	33.4
BCF	dB	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
BVR - Floor to Floor	dB	-6.0	-6.0	-6.0	-6.0	-6.0	-6.0	-6.0	-6.0	-6.0	-6.0	-6.0	-6.0	-6.0	-6.0	-6.0	-6.0	-6.0	-6.0	-6.0
BVR - Resonance	dB	2.0	3.0	4.0	5.0	6.0	6.0	6.0	6.0	5.8	5.6	5.4	5.2	5.0	4.0	3.0	2.0	1.3	0.7	0.0
CTN	dB	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0
SAF	dB	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0
Predicted Noise Level	1/3 Oct (Linear), dB	57.6	53.8	51.0	51.6	59.5	54.4	57.7	62.4	68.8	56.3	53.6	41.6	43.0	45.9	44.8	37.2	39.9	43.3	39.4
Noise Level	1/3 Oct (A-weighted), dBA	-12.8	-16.6	-12.4	-5.1	9.0	9.7	18.3	27.8	38.6	30.1	31.1	22.5	26.9	32.5	33.9	28.6	33.3	38.5	36.2
Predicted Noise Leq (Double Passby)	dBA	45 dBA																		
Predicted Noise Lmax, slow	dBA	45 dBA																		
Predicted Leq (30min, Night-time)	dBA	35 dBA (Criteria: 45 dBA)																		

Note: Speed correction has been included in the FDL for the operational groundborne noise assessment.

Figure B.1

Sample GBN Calculation based on Q-stock FDL at Hongway Garden of WIL

Date 4 July 2018

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